

SERIES
SLURRY/IS





INTRODUCTION

In this catalogue the entire range of pump models from the series IS produced by our company are described.

It contains technical information about construction, and characteristic curves from each model. Imbil and its DISTRIBUTORS will always be at your disposal to supply for additional information and to offer technical assistance.

NOTES

- We reserve the right to perform modifications in our products whenever necessary and this shall not incur in obligations of any type.
- The illustrations contained in this catalogue are indicative and in case there are any questions about their interpretation you must consult the DISTRIBUTOR IMBIL.



APPLICATION RANGE

Imbil's pumps are recommended for pumping liquids containing small or large suspended solid particulate, provided that said particulate pass through rotor's maximum opening. Said particulates may be large or small concentrations of coal, sand, phosphate, rocks, bauxite, minerals in general, ashes, rejects, and also abrasive and/or corrosive liquid.

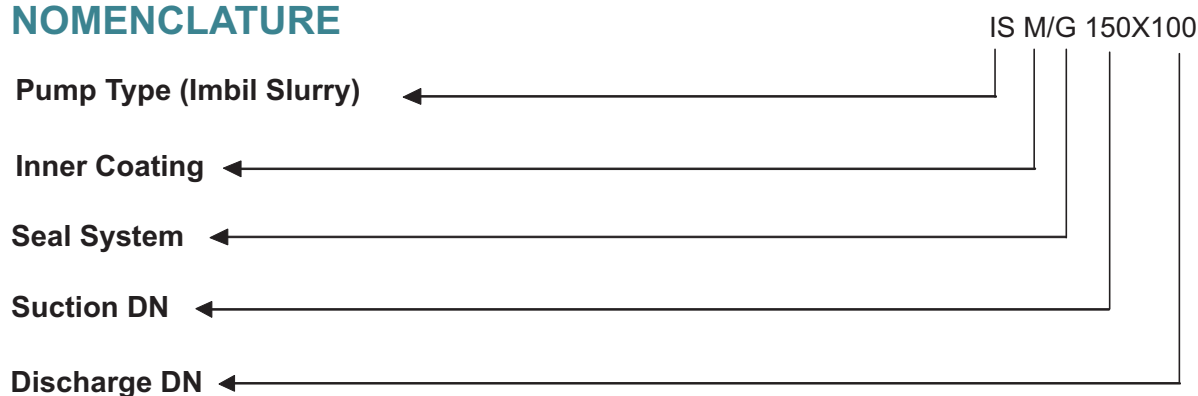
TYPICAL APPLICATIONS

Mining, steel mills, thermal power plants, sand processing, quarries, , fertilizers, chemical industry, sugar mills, ethanol destileries.

BASIC APPLICATIONS

Radially split horizontal coiled body, with simple suction rotor, high performance and excellent wear resistance for a wide operational range.

NOMENCLATURE



INNER COATING

M – Coated Pump with metal parts (High Chrome, AISI 316, CD4Mcu)

B – Coated Pump with elastomeric parts (Natural Rubber, Clorobil)

SEAL SYSTEM

G – Seal system with gland and gaskets

E – Seal system with centrifugal seal (Expeller)

M – Seal system with mechanical seal



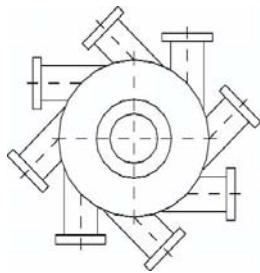
DRIVE

Driven by pulleys and belts, unless in some applications that may use flexible coupling (depending on required rotation), by electric motor, engine, turbines, etc.

ROTATION DIRECTION

Clockwise sense rotation, from the drive side

OUTLET FLANGE ALTERNATE POSITIONS



View
(From the Suction Flange)

From the normal upwards position, the outlet flange may be rotated each 45°. Not all the above outlet positions are enabled; they depend on motor assembly setting.

BEARING LUBRICATION

Bearing is lubricated with lithium-base, mineral oil grease.



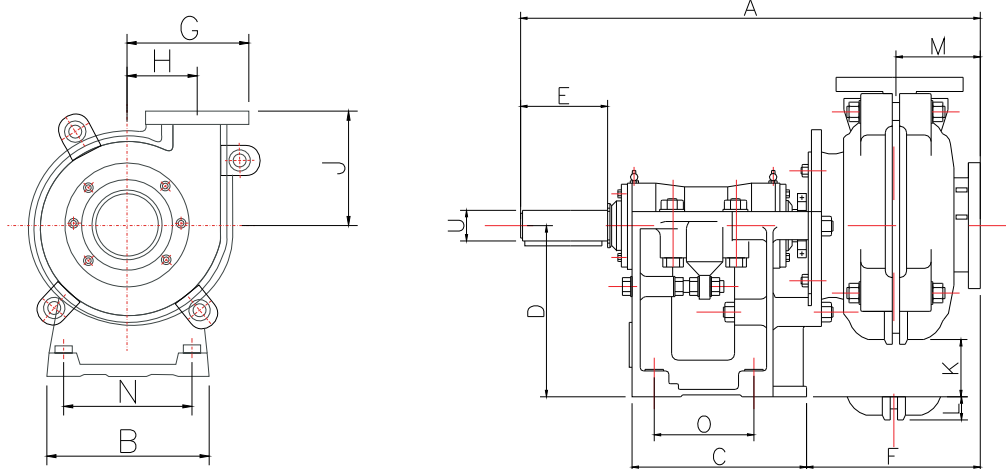
SEALING WATER

Pumps sealed with gaskets shall be injected with clean water to prevent solid particulate from penetrating, and also to cool down and lubricate the gasket.

The seal water pressure shall be 0.34 kgf/cm² to 0.7 kgf/cm² above pump's outlet pressure.
Seal water flow is shown for each model in below table:

SIZE	FLOW	
38x25	0,9 m ³ /h	4 GPM (US)
50x38	0,9 m ³ /h	4 GPM (US)
75x50	1,98 m ³ /h	9 GPM (US)
100x75	1,98 m ³ /h	9 GPM (US)
150x100	2,52 m ³ /h	11 GPM (US)
200x150	2,52 m ³ /h	11 GPM (US)
250x200	6,00 m ³ /h	26 GPM (US)
300x250	6,00 m ³ /h	26 GPM (US)
350x300	6,00 m ³ /h	26 GPM (US)

OUTLINE DIMENSIONS



MODEL	A	B	C	D	U	KEY	E	F	G	H	J	K	L	WEIGHT M B		M	N	O
38x25	583	295	248	197	28	8x7	79	207	182	98	171	46	-	85	73	109	258	144
50x38	592	295	248	197	28	8x7	79	217	203	114	184	83	-	95	80	112	258	144
75x50	768	406	310	254	42	12x8	121	280	238	138	210	71	-	180	150	154	348	171
100x75	843	406	310	254	42	12x8	121	353	292	149	262	24	-	295	215	187	348	171
150x100	1171	622	448	457	82	22x16	222	433	406	229	338	138	-	785	615	220	545	257
200x150	1292	622	448	457	82	22x16	222	557	550	318	460	90	-	1460	990	220	545	257
250x200	1748	1150	780	650	120	32x18	280	692	673	419	635	27	-	3430	2840	319	560	490
300x250	1816	1150	780	650	120	32x18	280	762	755	464	673	-	65	4190	3410	381	900	620
350x300	1873	1150	780	650	120	32x18	280	812	937	629	832	-	224	5870	4780	398	900	620

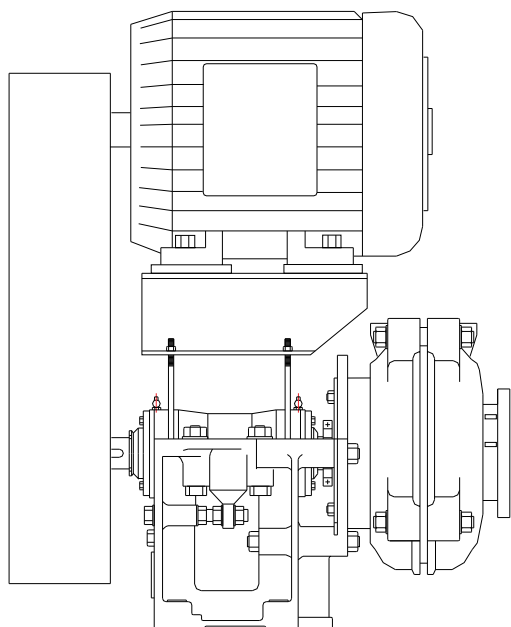
Notes: 1) Dimensions in [mm]

2) Dimensions and weight for information only,
do not use in design. Request a certified
drawing when required.

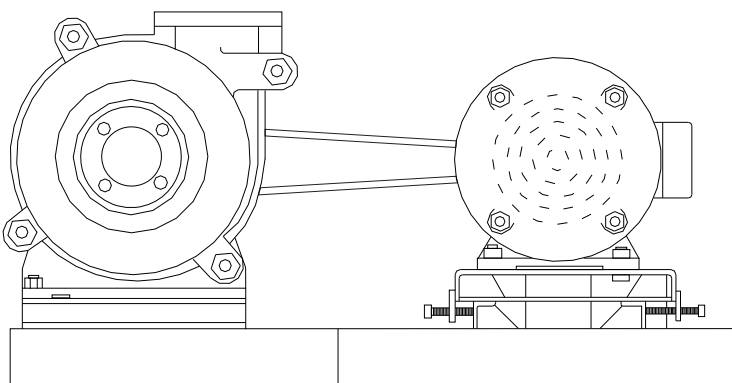
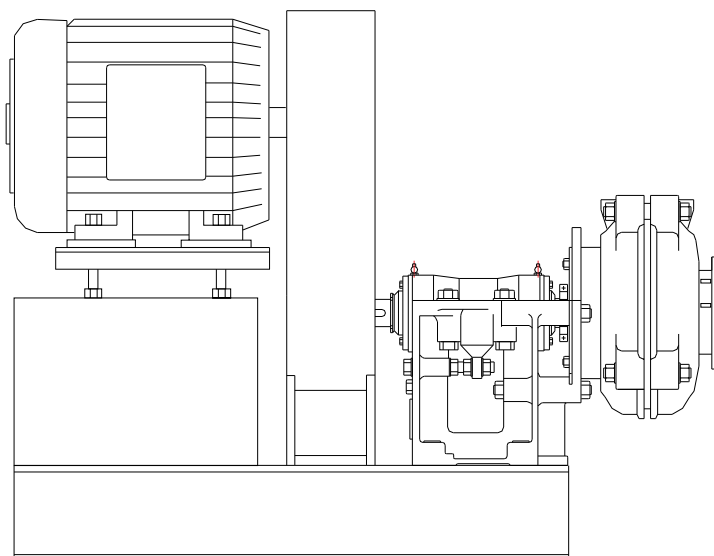


GENERAL ARRANGEMENT

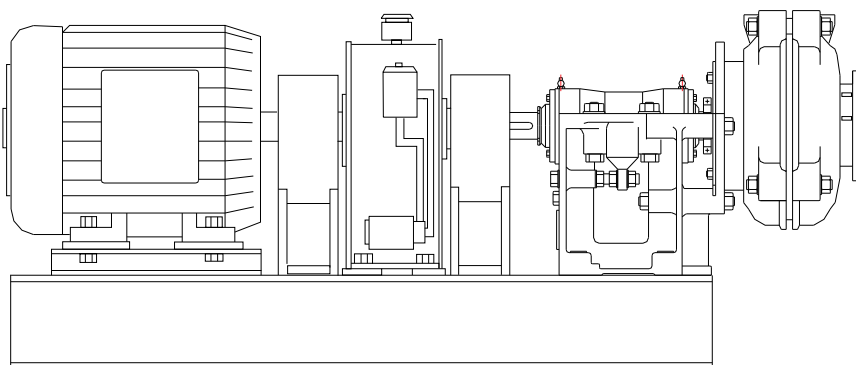
On Bearing Assembly



Behind / over the Bearing Assembly



Side mounting

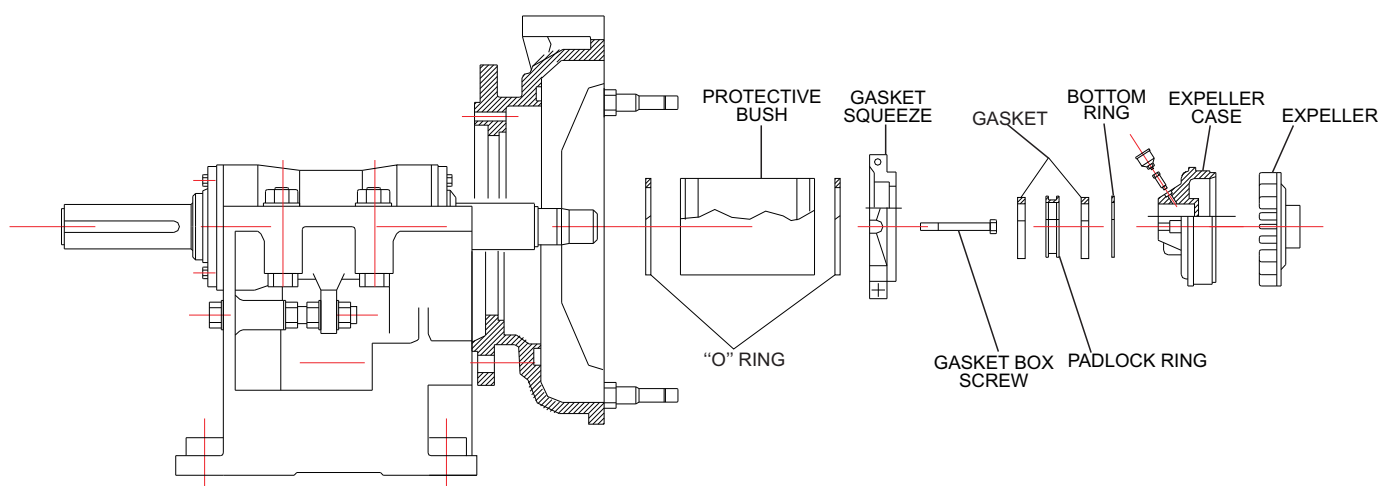


In-line mounting

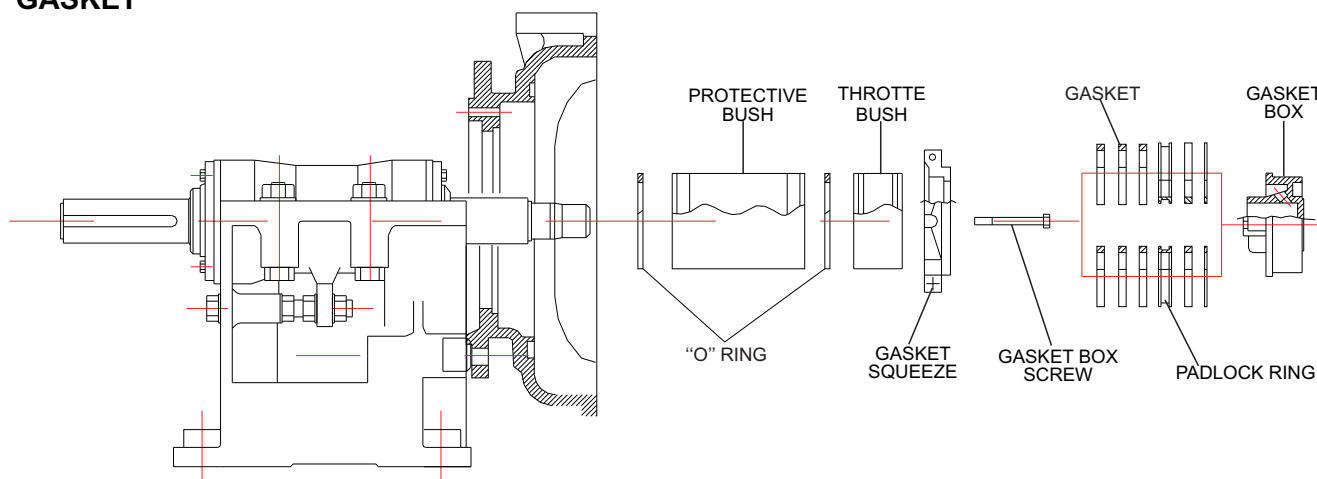


SEAL SYSTEM

EXPELLER



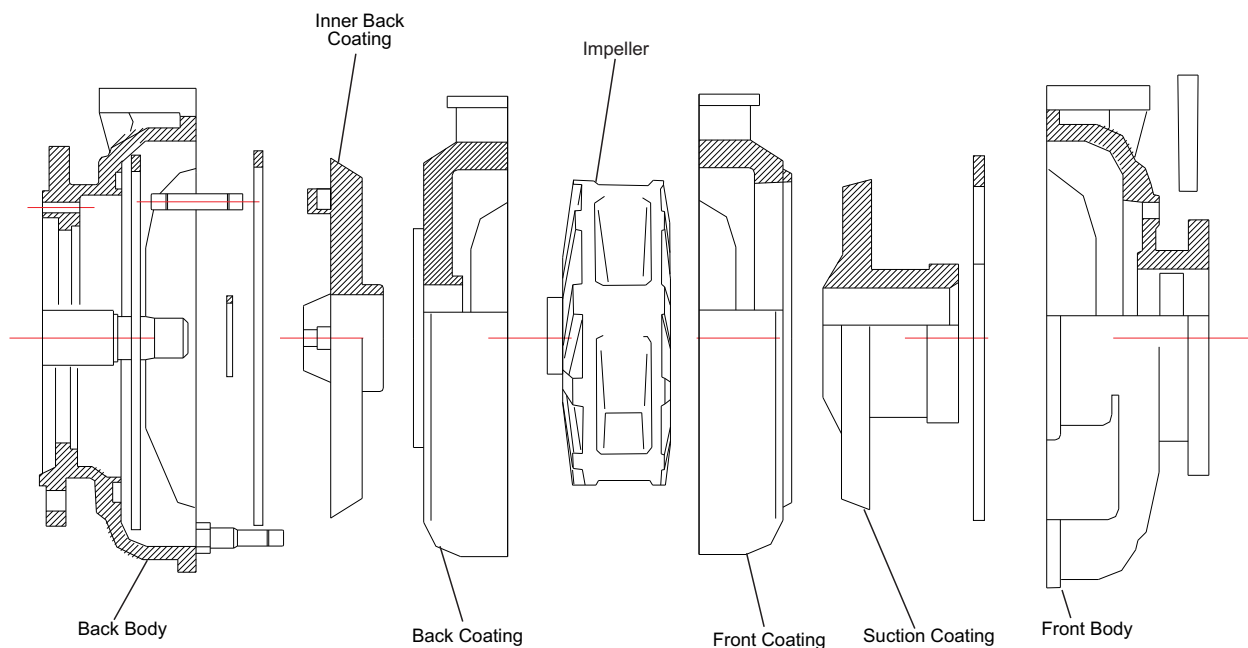
GASKET



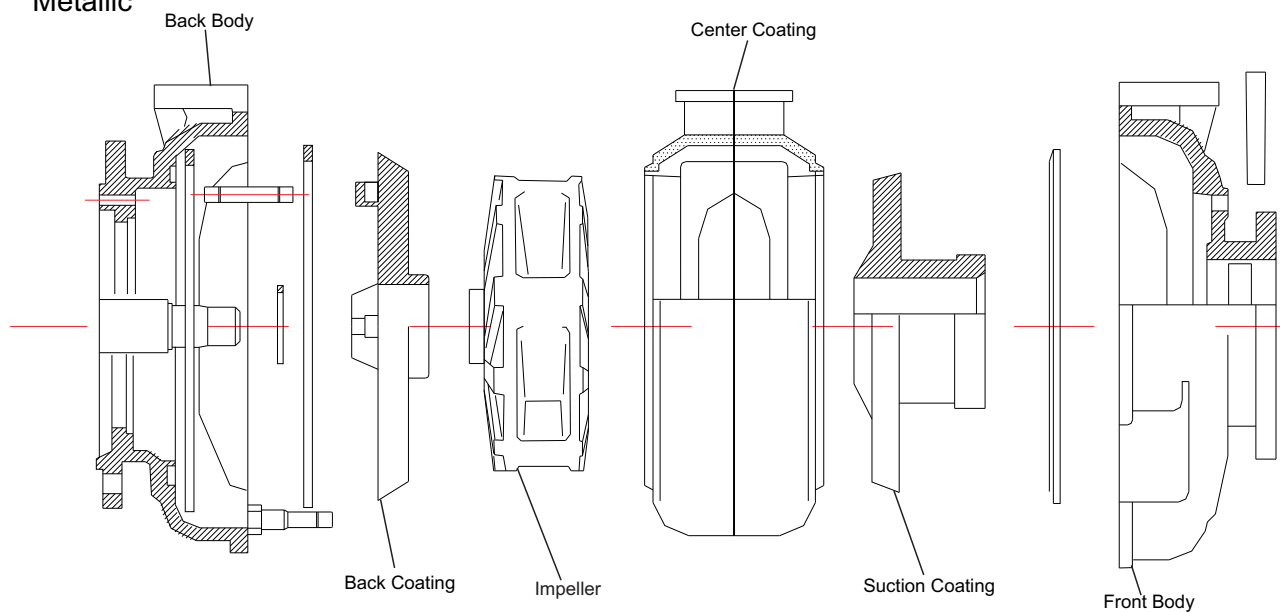


COATINGS

RUBBER

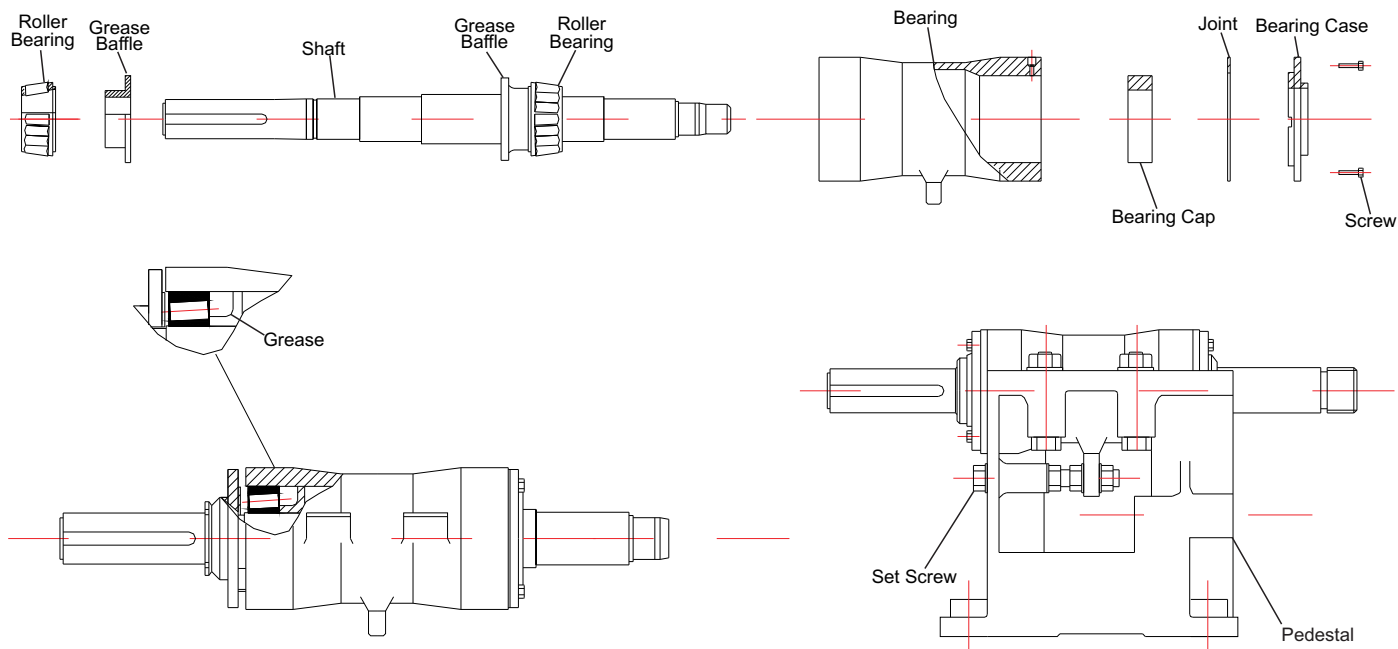


Metallic





BEARING ASSEMBLY



MATERIALS LIST		MATERIAL CODE		
Part Description	B1	B2	M1	M2
Front Body	ASTM A536 65.45.12	ASTM A536 65.45.12	ASTM A536 65.45.12	ASTM A536 65.45.12
Back Body	ASTM A536 65.45.12	ASTM A536 65.45.12	ASTM A536 65.45.12	ASTM A536 65.45.12
Impeller	Natural Rubber	Clorobutil	A 532 CL III TIPO A (NI-HARD)	CD4MCu
Inner Coating	Natural Rubber	Clorobutil	A 532 CL III TIPO A (NI-HARD)	CD4MCu
Expeller if applicable	Natural Rubber	Clorobutil	A 532 CL III TIPO A (NI-HARD)	CD4MCu
Expeller Case if applicable	ASTM A48 CL30	ASTM A48 CL30	A 532 CL III TIPO A (NI-HARD)	CD4MCu
Expeller Case Coating	Natural Rubber	Clorobutil		
Gaskets	PTFE/GRAFITE + ARAMIDA	PTFE/GRAFITE + ARAMIDA	PTFE/GRAFITE + ARAMIDA	PTFE/GRAFITE + ARAMIDA
Bearing Casel	ASTM A48 CL30	ASTM A48 CL30	ASTM A48 CL30	ASTM A48 CL30
Shaft	SAE 4140	SAE 4140	SAE 4140	AISI 316
Shaft sleeve	AISI 420	AISI 420	AISI 420	AISI 420
Roller Bearings	Carbon steel	Carbon steel	Aço Carbono	Aço Carbono
Pedestal	ASTM A48 CL30	ASTM A48 CL30	ASTM A48 CL30	ASTM A48 CL30

Remarks: Above materials are standard and may be changed depending on application.



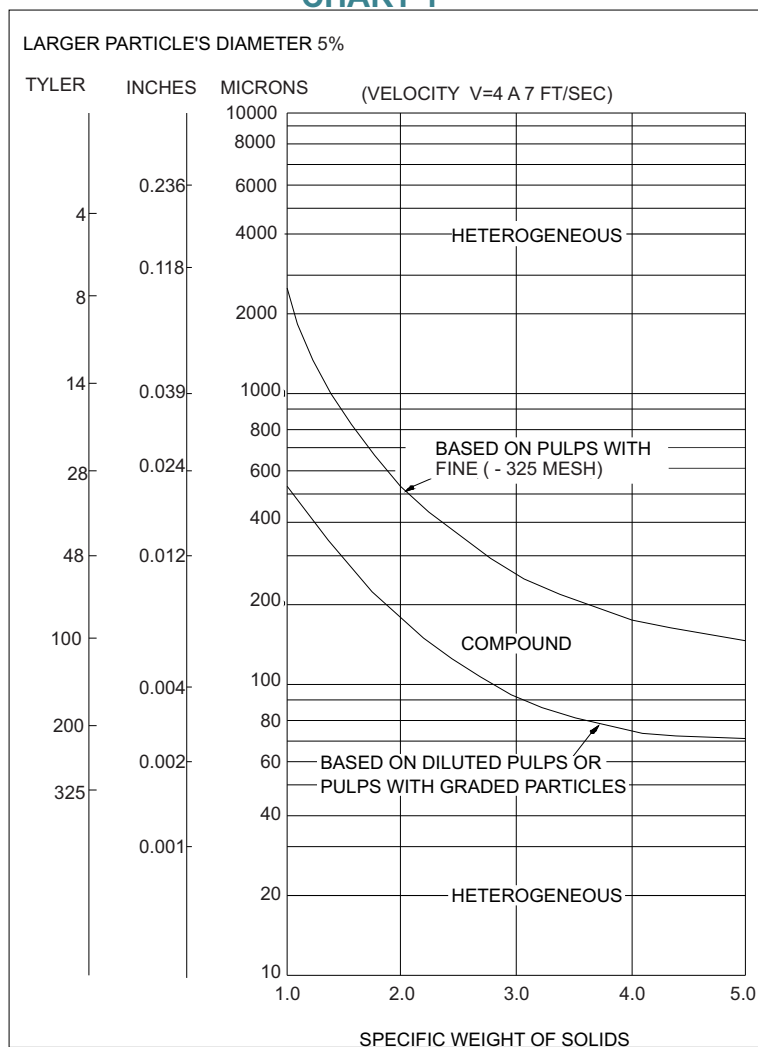
PULP LOAD LOSS CALCULATION CHARTS

Below charts are used to calculate the A.M.T. in liquid pumping systems with suspended solids.

Basic formulas: $S_m = \frac{SL + \frac{C_v}{100} (S - SL)}{1 - \frac{C_w}{100} \frac{(S - SL)}{S}}$; $C_w = \frac{C_v * S}{S_m} [\%]$; $C_v = \frac{(S_m - SL) * 100}{(S - SL)} [\%]$

Where: D_m = Pulp Density; SL = Liquid Density [t/m^3]; S = Actual Solids Density [t/m^3]
 C_v = Solids concentration in volume; C_w = Solids concentration in weight.

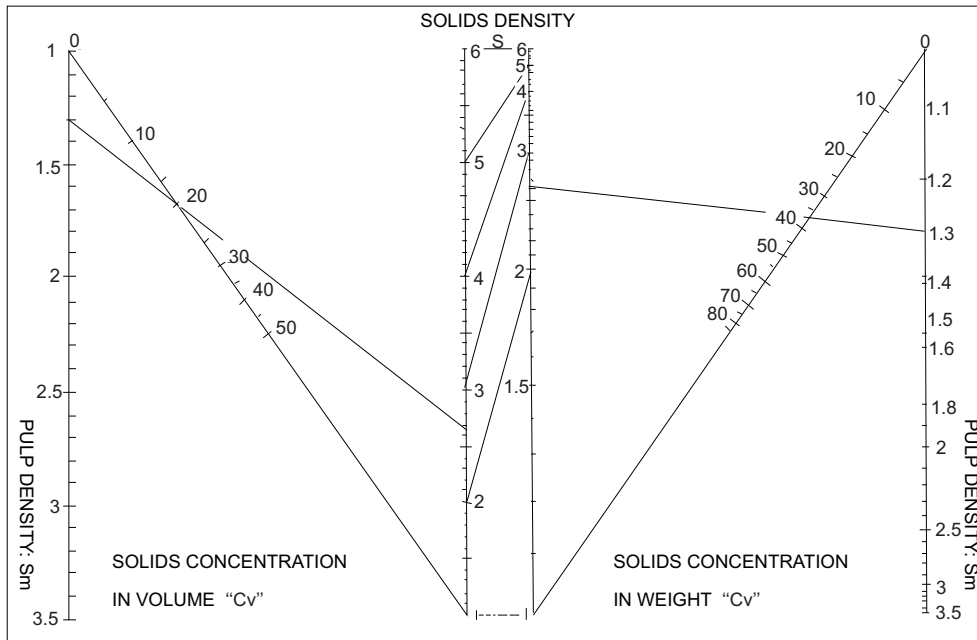
CHART 1



Pulp flow system (heterogeneous, homogeneous) is a function of solids specific size and weight

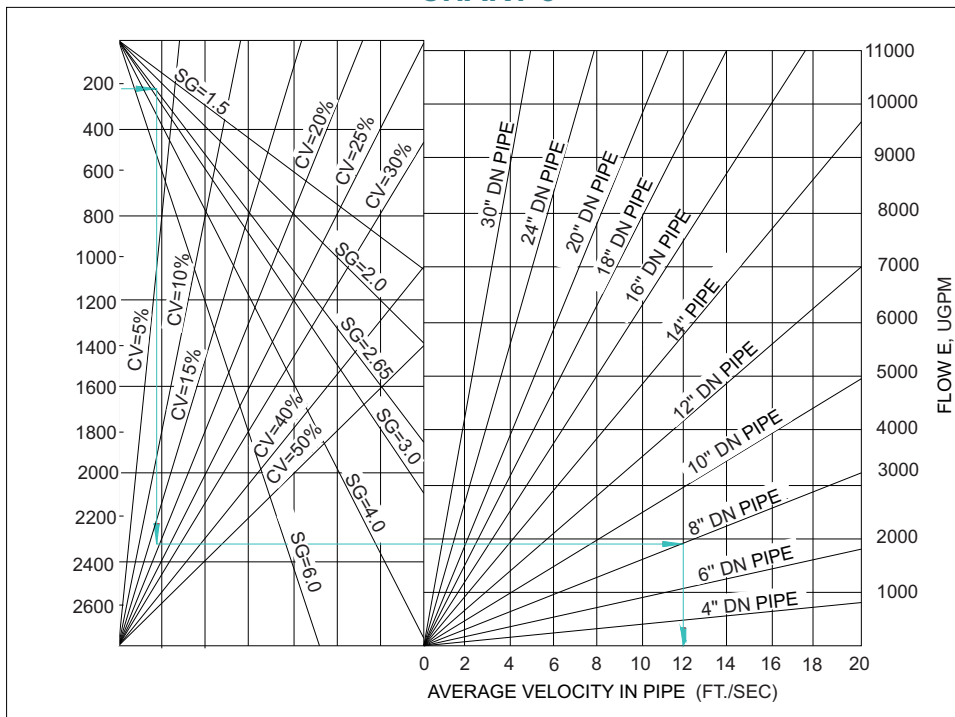


CHART 2



Pulp density chart to mix water and solids.

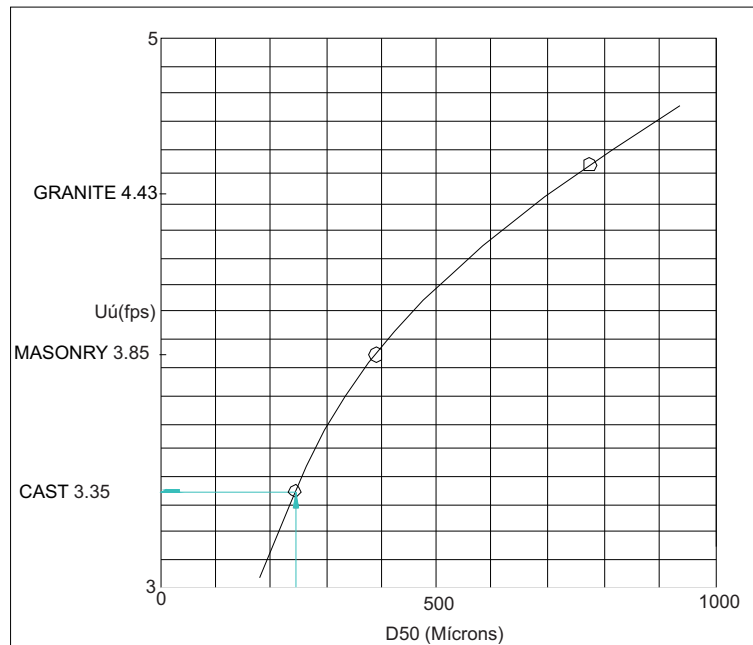
CHART 3



Average velocity of pulp inside piping, given dry solids flow, solids density, solids concentration in volume and pipe diameter

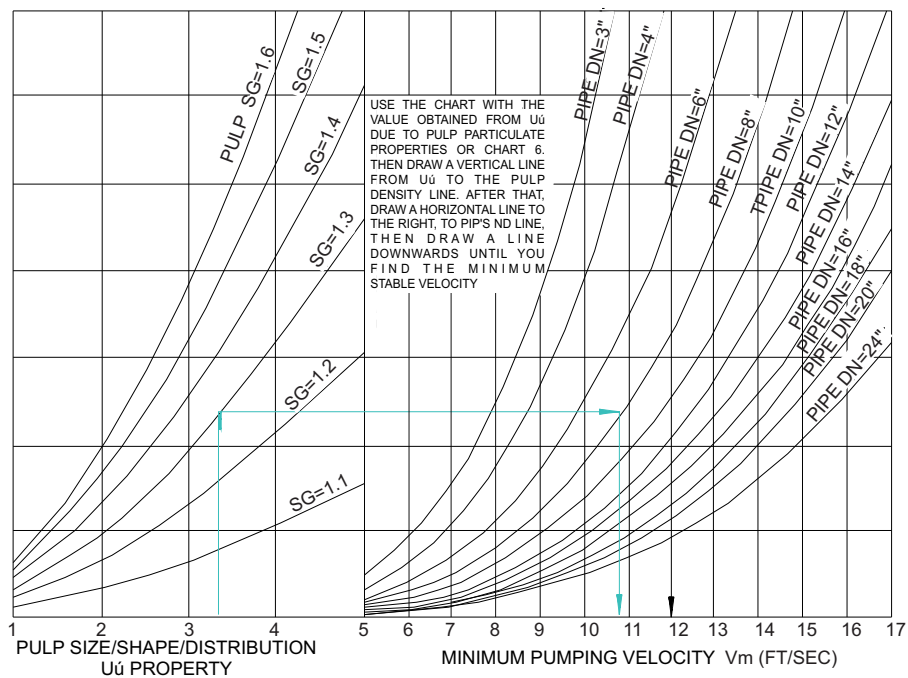


CHART 4



Sand $U_{\text{ú}}$ [??] value without silt or clay components.

CHART 5



stable pumping velocity for pulps that settle in heterogeneous flow (smooth/soft pipe)



CHART 6

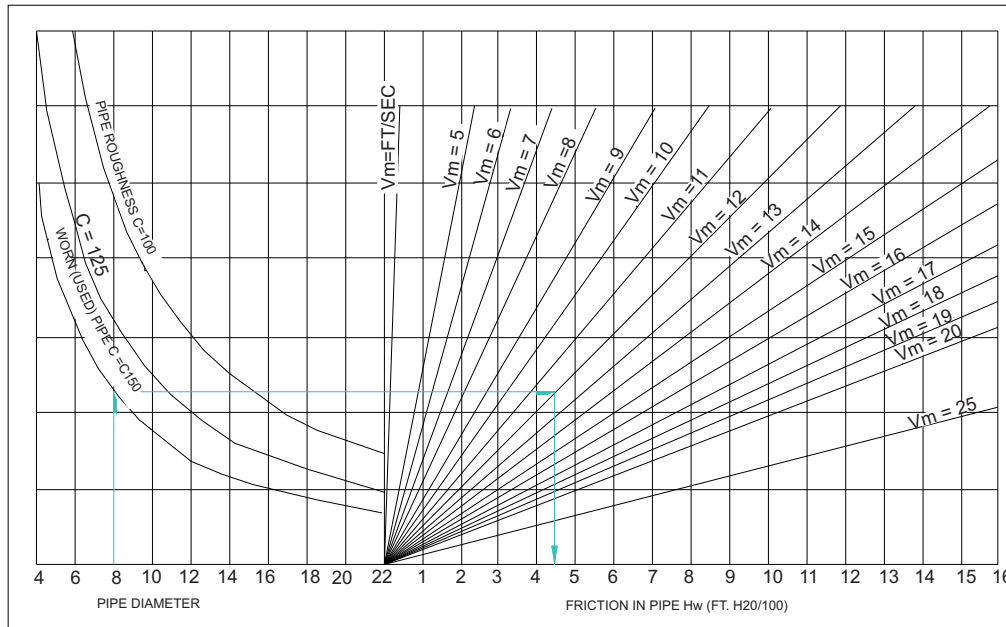


CHART 7

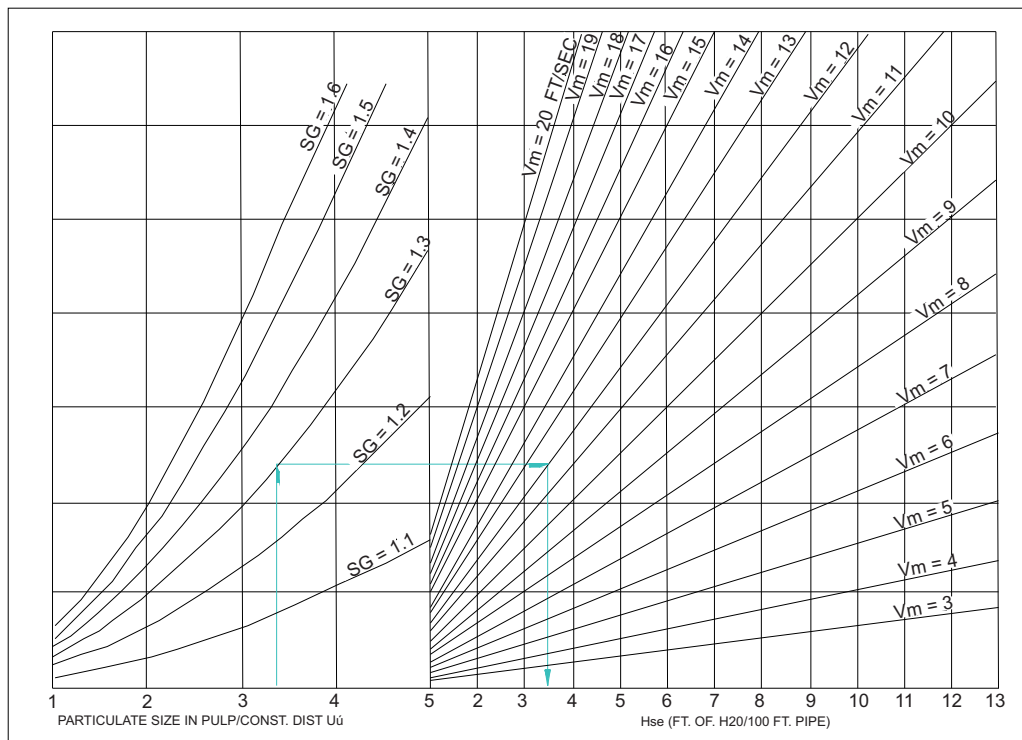




CHART 8

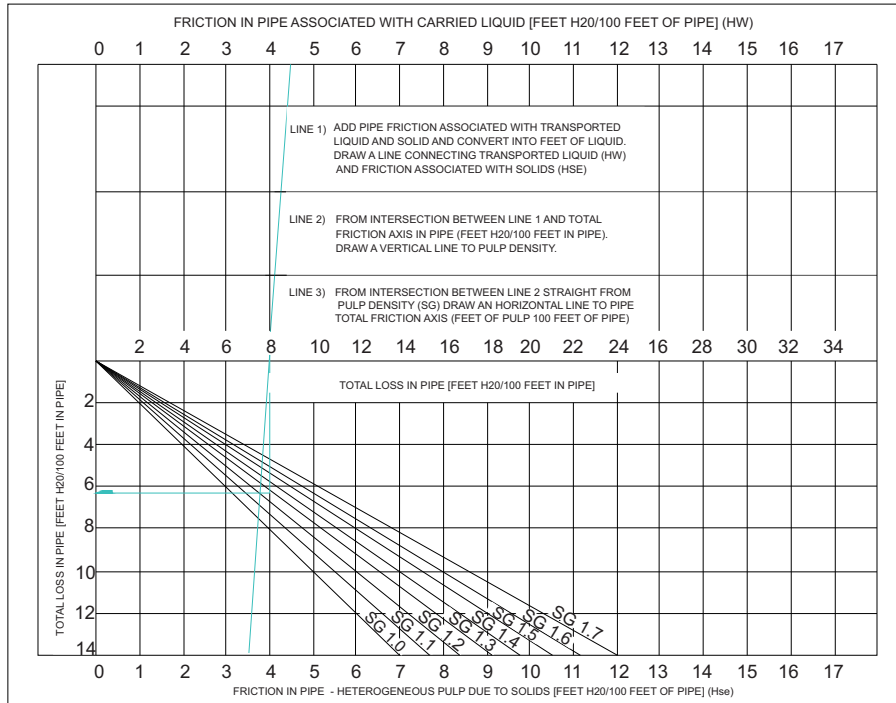
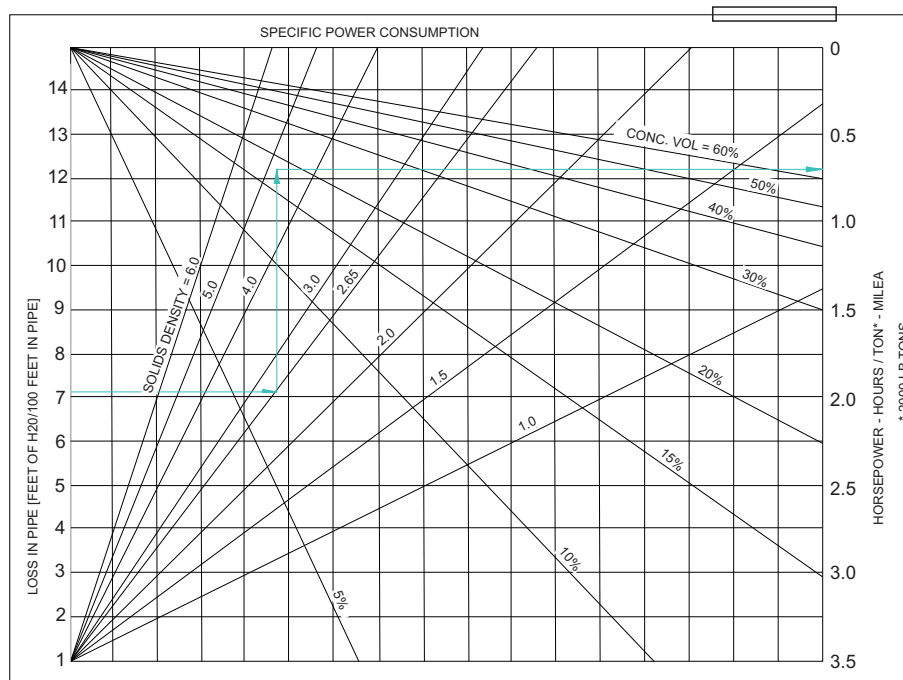


CHART 9





EXAMPLE

Calculate the load loss to carry 225 t/h of foundry sand, being $S = 2.65 \text{ t/m}^3$, $S_m = 1.3$ and $D_{50} = 240$ microns along a horizontal pipe with 8" internal diameter.

Chart 1) The pulp can be treated as sedimentary solids pulp.

Chart 2) With $S \times S_m$ we find $C_v = 18\%$ and $C_w = 37\%$.

Chart 3) With 225 t/h draw a straight line (1) horizontally to curve $S = 2.65$, then draw a straight line (2) vertically to curve $C_v = 18\%$, then draw a straight line (3) horizontally to 8" pipe ND curve, then draw a straight line (4) to average velocity axis on pipe, which is 12 feet/s.

Chart 4) With $D_{50} = 240$, draw a vertical line to curve and then draw a horizontal line to U_u axis to find $U_u = 3.35$.

Chart 5) With $U_u = 3.35$ draw a straight line (1) vertically to curve $S_m = 1.3$, then draw a straight line (2) to curve ND 8", then draw a straight line (3) to minimum pumping velocity axis to find $V_m = 10.8$ feet/sec. As the average velocity in pipe found in chart (3) is 12 feet/sec, this is OK (12 feet/sec > 10.8 feet/sec OK)

Chart 6) With DN 8", draw a straight line (1) vertically to smooth (used) pipe curve $C = 150$, then draw a straight line (2) horizontally to curve $V_m = 12$ feet/sec, then draw a straight line (3) vertically to friction axis in pipe H_w to find $H_w = 4.4$ feet of $H_2O/100$ feet of pipe.

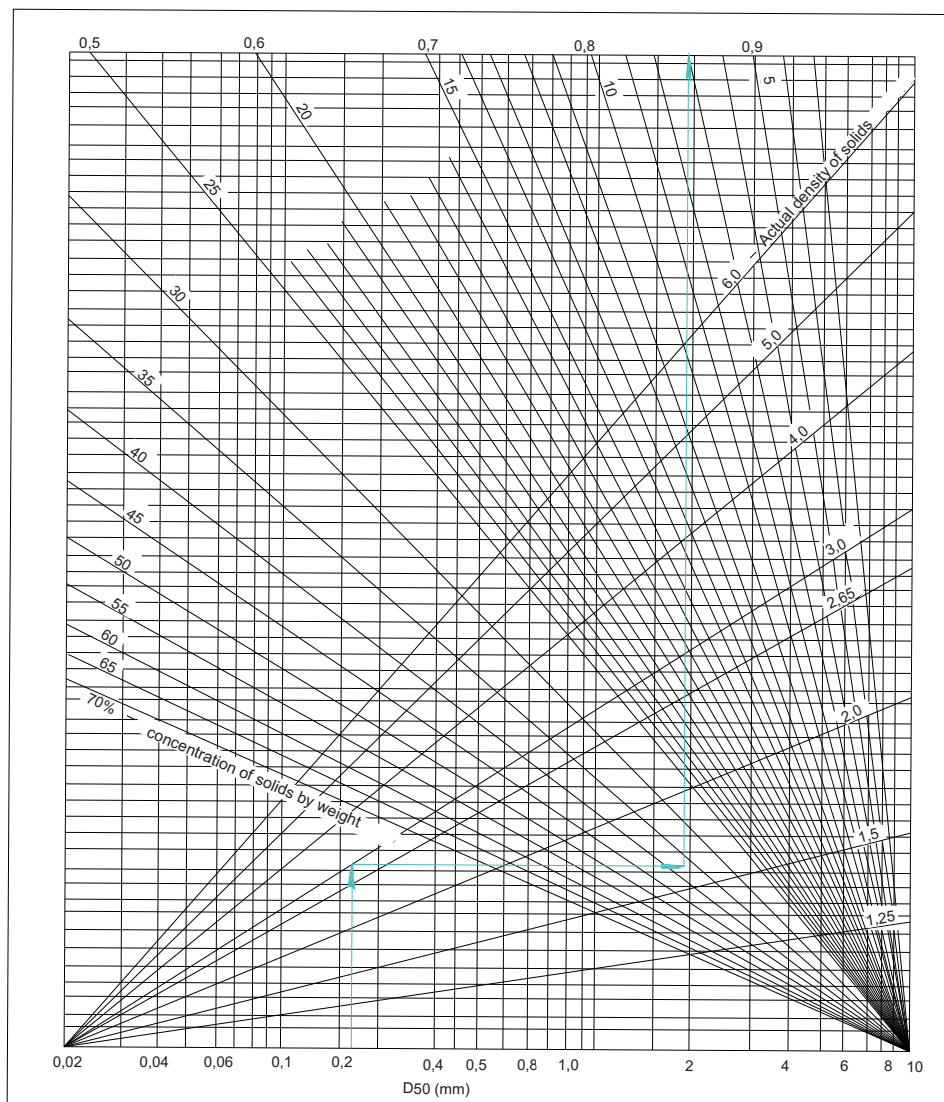
Chart 7) With $U_u = 3.35$, draw a straight line (1) vertically to curve $S_m = 1.3$, then draw a straight line (2) horizontally to curve $V_m = 12$ feet/sec, then draw a straight line (3) vertically to friction axis H_{se} to find $H_{se} = 3.6$ feet of $H_2O/100$ feet of pipe.

Chart 8) With values of charts 6 and 7, respectively $H_w = 4.4$ feet of $H_2O/100$ feet of pipe and $H_{se} = 3.6$ feet of $H_2O/100$ feet of pipe we find the total load loss 6.15 feet of pulp/100 feet of pipe. See instructions on how to use the chart on the chart body itself.

Chart 9) With the value obtained from chart (8), draw a straight line (1) horizontally to curve $S = 2.65 \text{ t/m}^3$, then draw a straight line (2) vertically to curve $C_v = 18\%$, then draw a straight line (3) to Horsepower axis to find 0.687 HP-Hour/Ton-Mile.



HR and ER CALCULATION CHART



- 1) The next chart is used to adjust the total manometer height and pump efficiency when the pump works with liquids containing suspended solids (pulpes).
- 2) Characteristic curves shown on this catalogue were produced in water, therefore adjustments are required.
- 3) How to Use the Chart Using the previous example, i.e., $D_{50}=240$ microns = 0.24 mm, solid density $S=2.65$ t/m³ and solid concentration in weight $C_w=37\%$.
From D_{50} axis, draw a straight line (1) vertically to solid density curve $S=2.65$ t/m³, then draw a straight line (2) to solid concentration in weight curve C_w 37%, then draw a straight line (3) vertically to axis HR-ER to find the value of $HR=ER=0.86$.

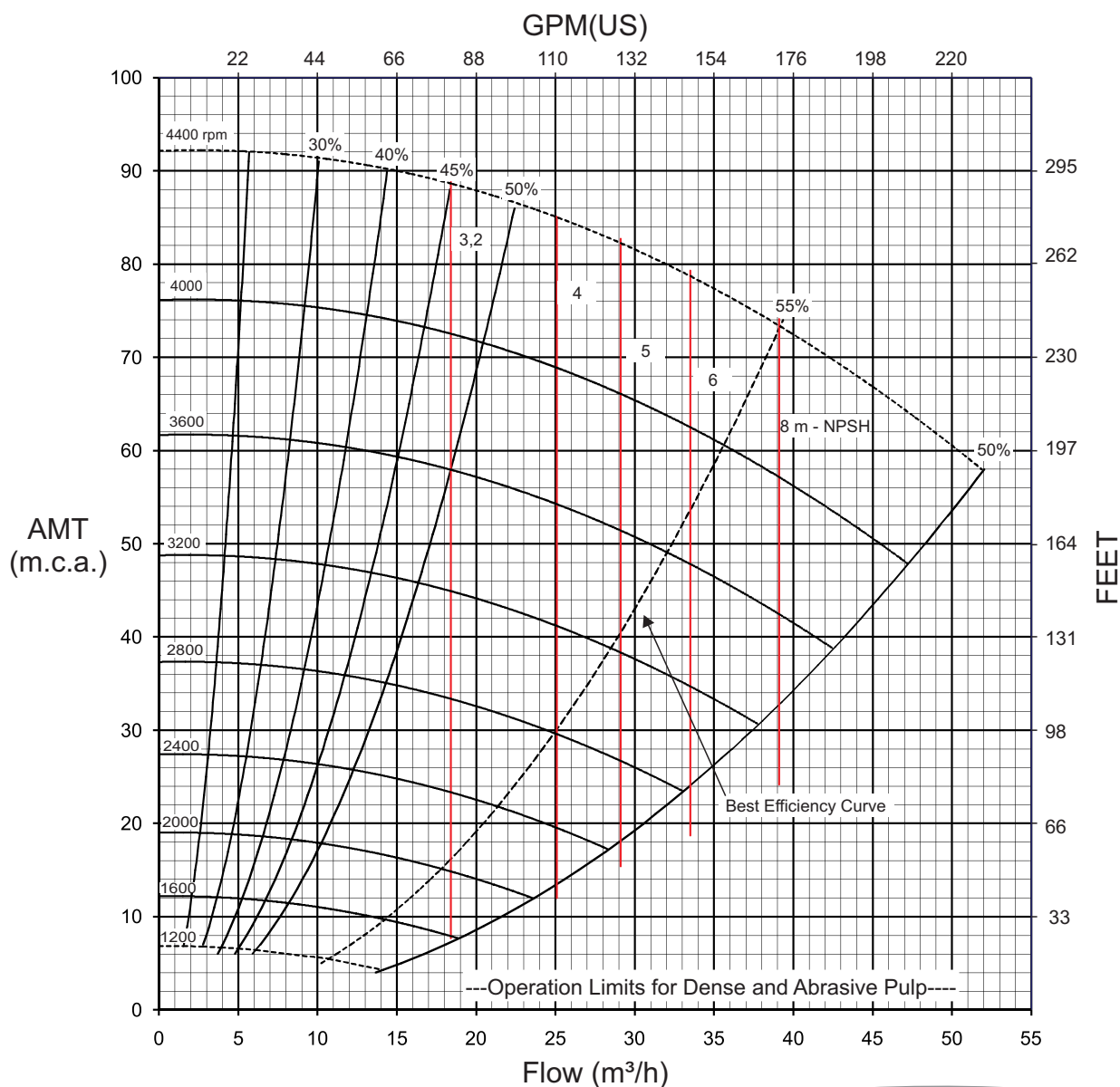


MODEL PUMP

IS M/G 38X25

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	38 mm	ND	152 mm
ND Discharge	25 mm	Type	Open
Material	Cast Iron	Material	Metal
Coating	Metal/Rubber	Free Passage	14 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____ with Q_m and H_w we find the efficiency in water E_w _____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			



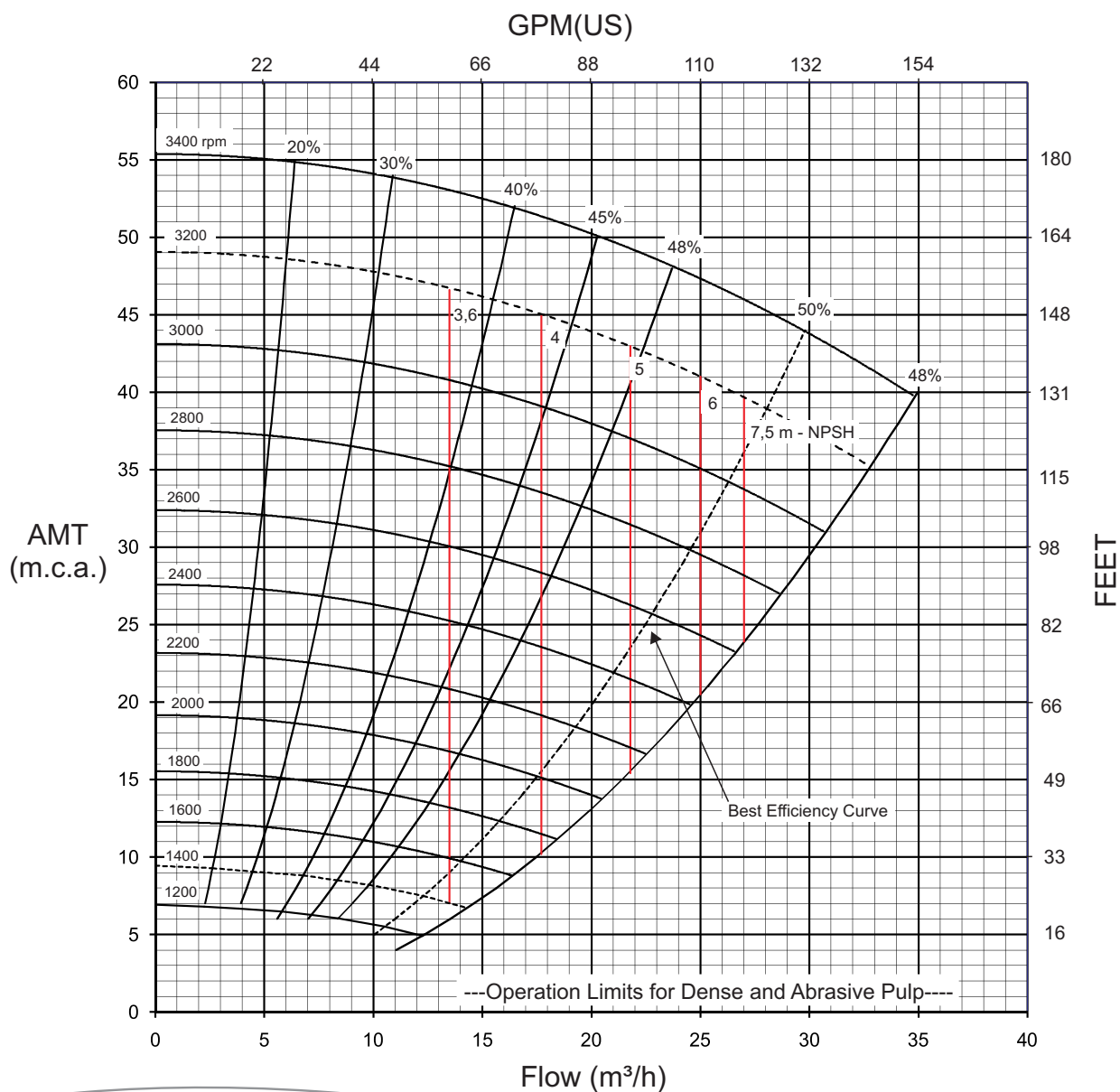


MODEL PUMP

IS B/G 38X25

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 3 Blades	
ND Suction	38 mm	ND	152 mm
ND Discharge	25 mm	Type	Open
Material	Cast Iron	Material	Rubber
Coating	Metal/Rubber	Free Passage	20 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____ with Q_m and H_w we find the efficiency in water E_w _____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			

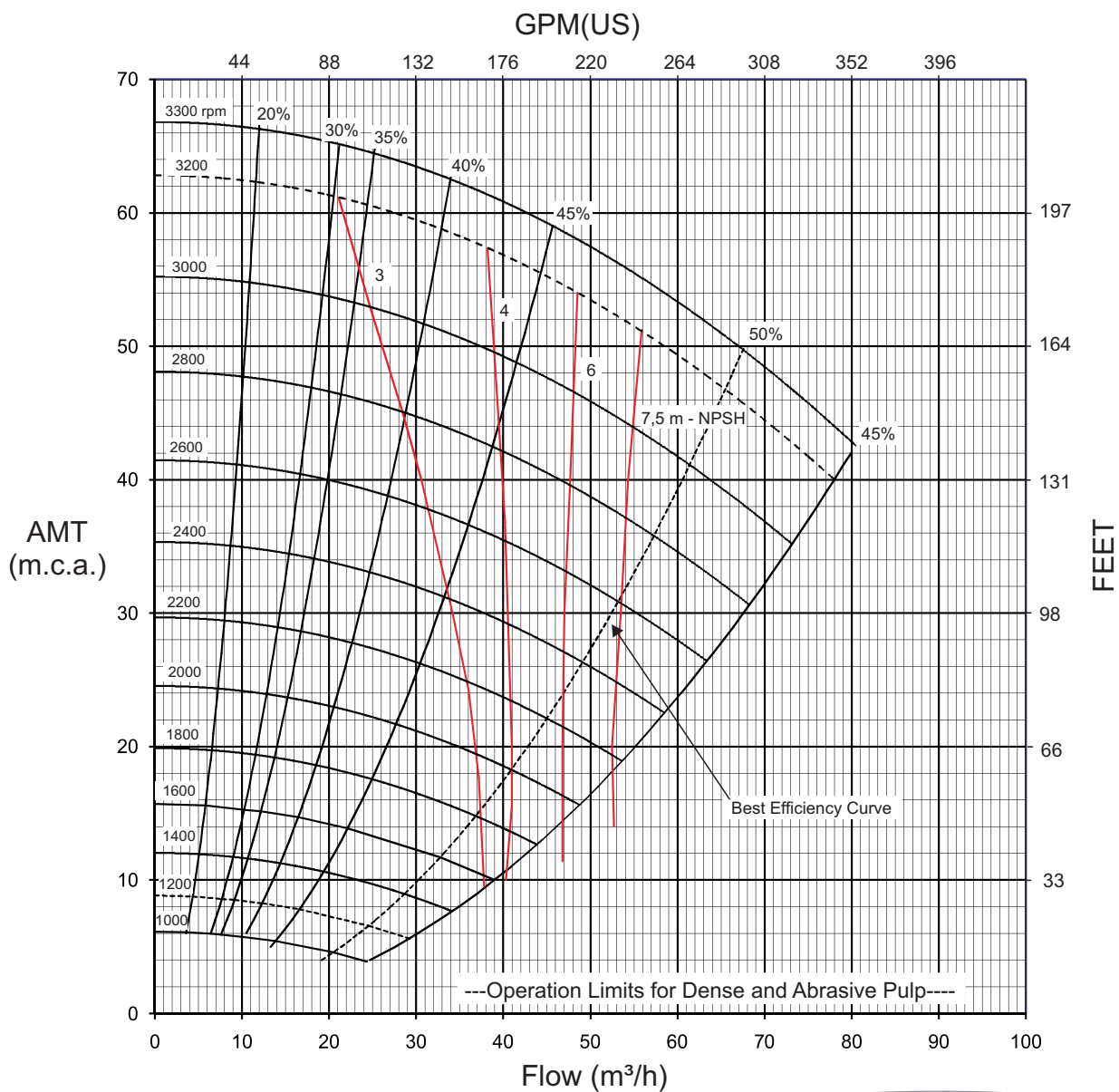


IS M/G 50X38

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	50 mm	ND	184 mm
ND Discharg	38 mm	Type	Open
Material	Cast Iron	Material	Metal
Coating	Metal/Rubber	Free Passage	19 mm

POWER CALCULATION	
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____. with Q_m and H_w we find the efficiency in water E_w ____ Through BHP = $(\frac{Q_m \times H_m \times S_m}{270 \times E_w \times ER})$, we find power BHP- _____ - _____ hp	
Where: H_w =AMT in Water, H_m -AMT in Pulp	





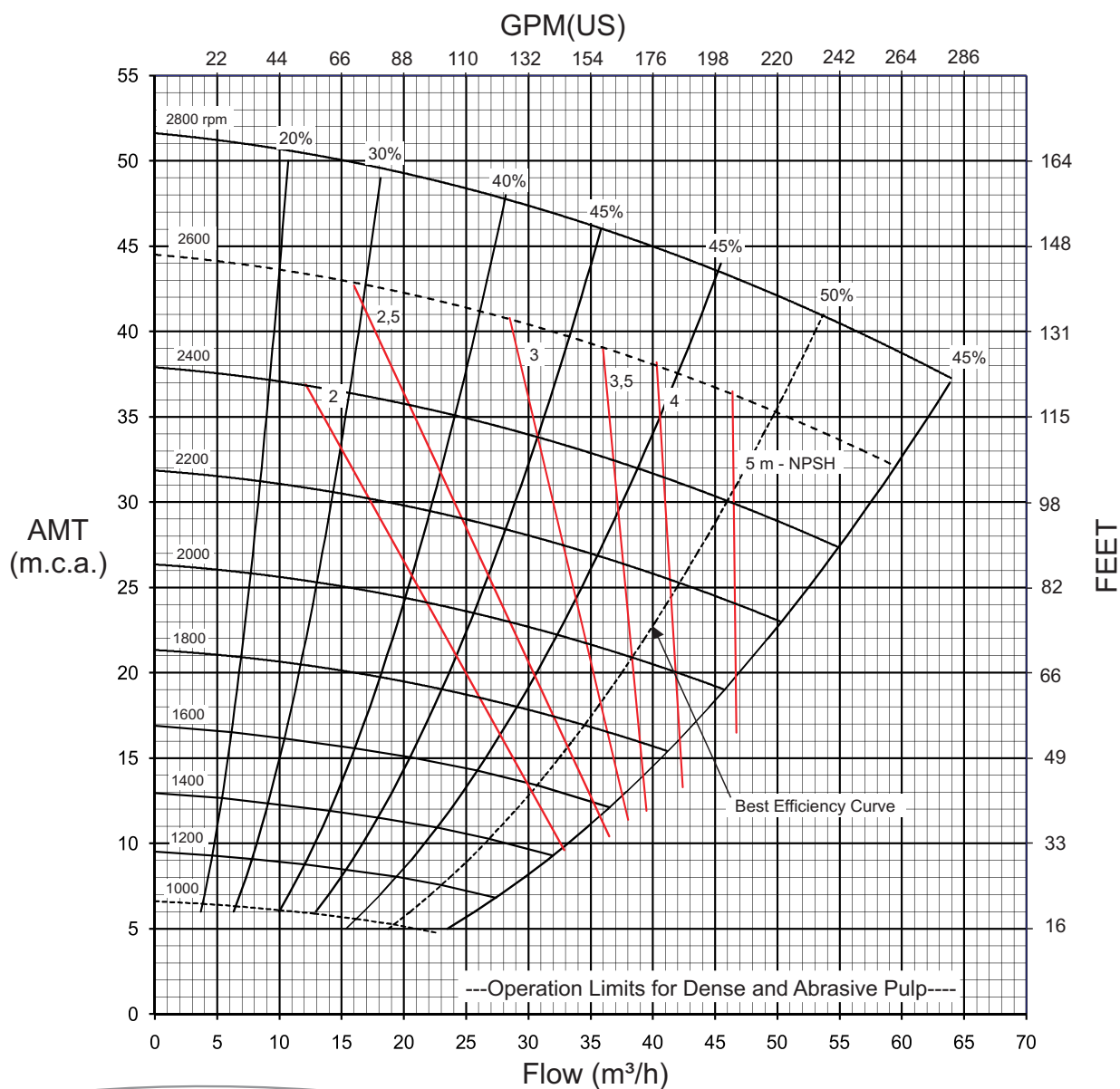
MODEL PUMP

IS B/G 50X38

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	50 mm	ND	180 mm
ND Discharge	38 mm	Type	Open
Material	Cast Iron	Material	Rubber
Coating	Metal/Rubber	Free Passage	16 mm

POWER CALCULATION	
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____. with Q_m and H_w we find the efficiency in water E_w ____ Through $BHP = (Q_m \times H_m \times S_m) / (270 \times E_w \times ER)$, we find power BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp	



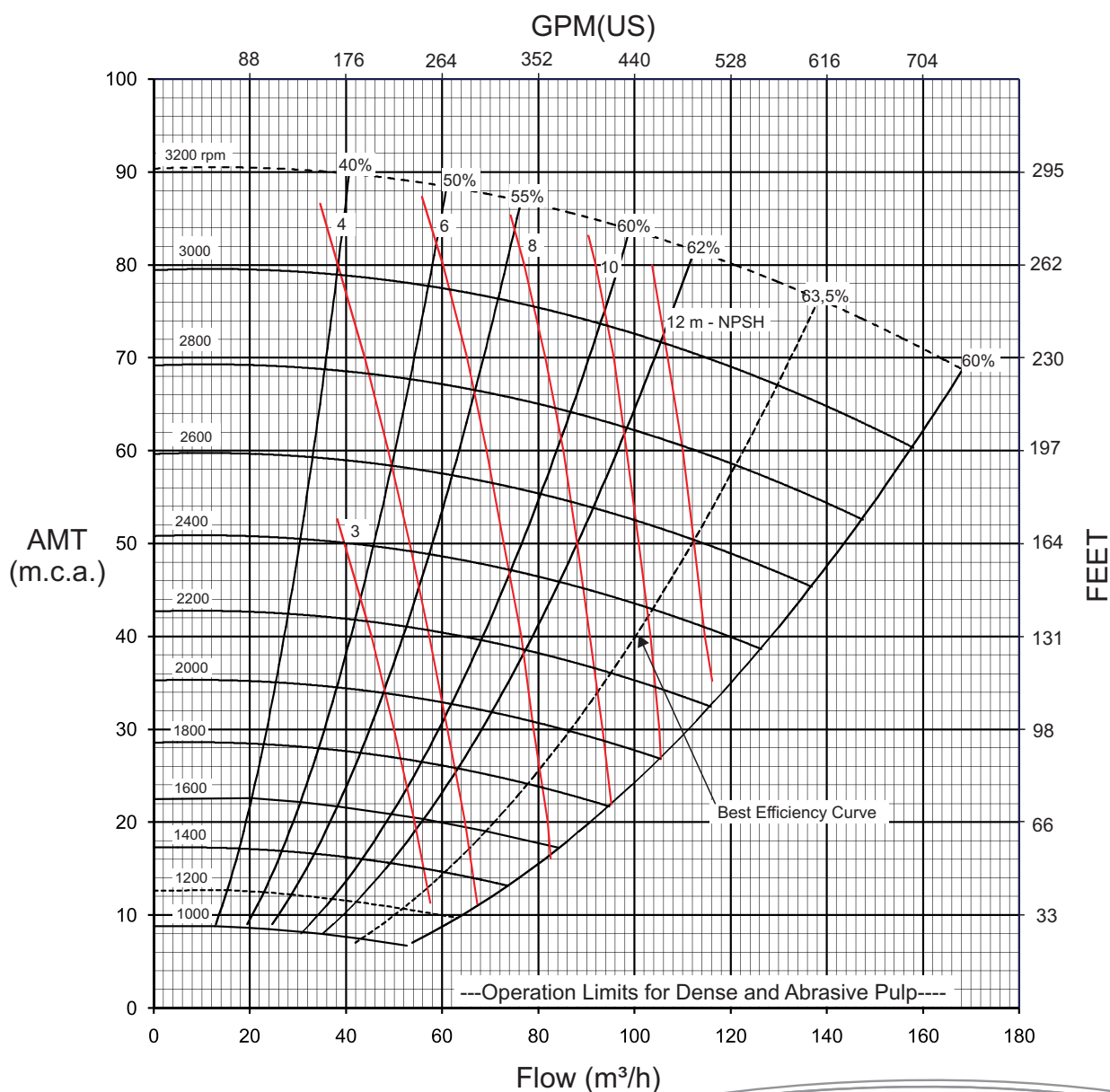


MODEL PUMP

IS M/G 75X50

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	75 mm	ND	214 mm
ND Discharge	50 mm	Type	Close
Material	Cast Iron	Material	Metal
Coating	Metal/Rubber	Free Passage	25 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____. with Q_m and H_w we find the efficiency in water E_w ____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			



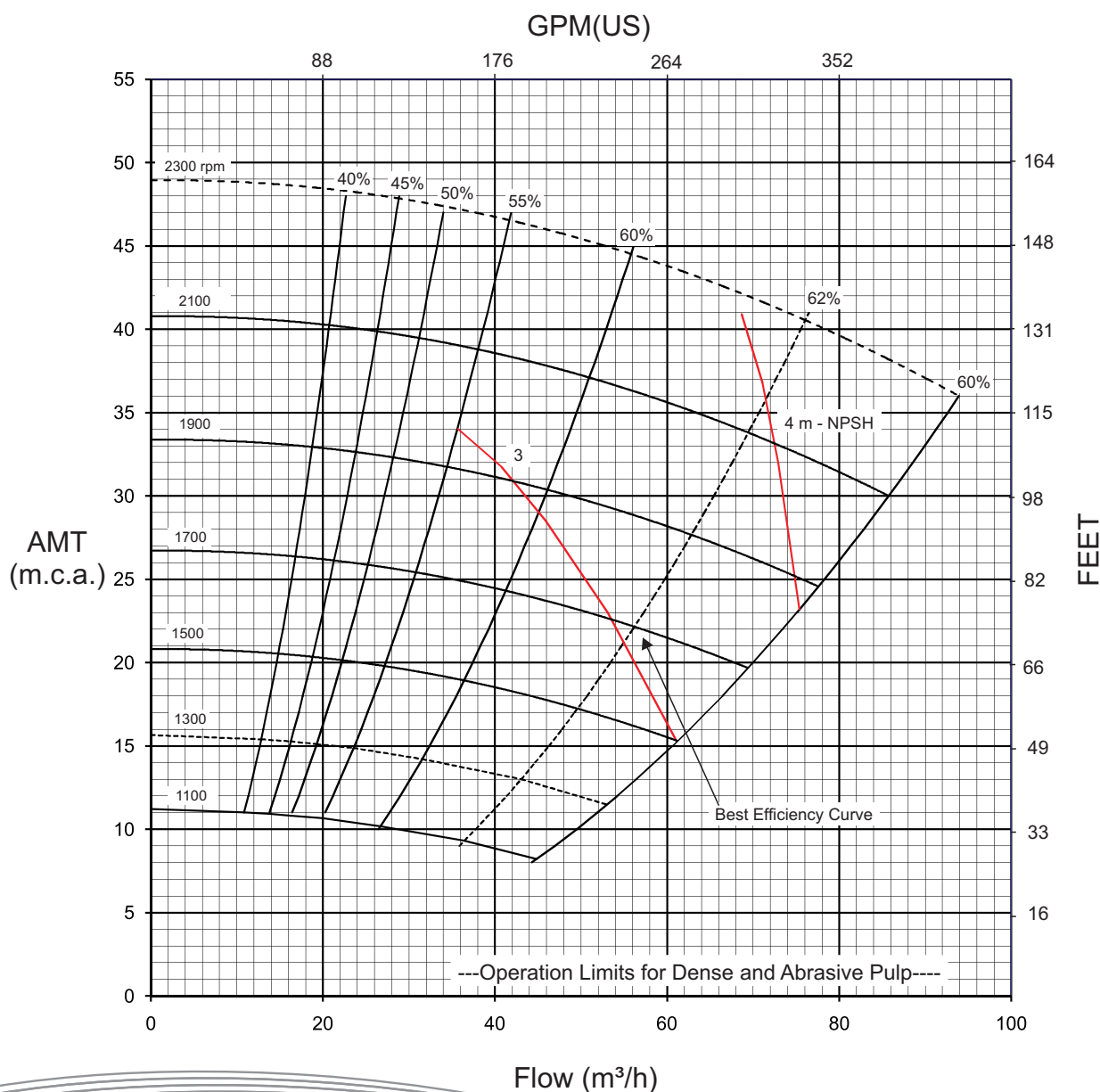


MODEL PUMP

IS B/G 75X50

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	75 mm	ND	215 mm
ND Discharg	50 mm	Type	Open
Material	Cast Iron	Material	Rubber
Coating	Metal/Rubber	Free Passage	21 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m/HR = \text{_____} / \text{_____}$, H_w - _____. with Q_m and H_w we find the efficiency in water E_w ____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			



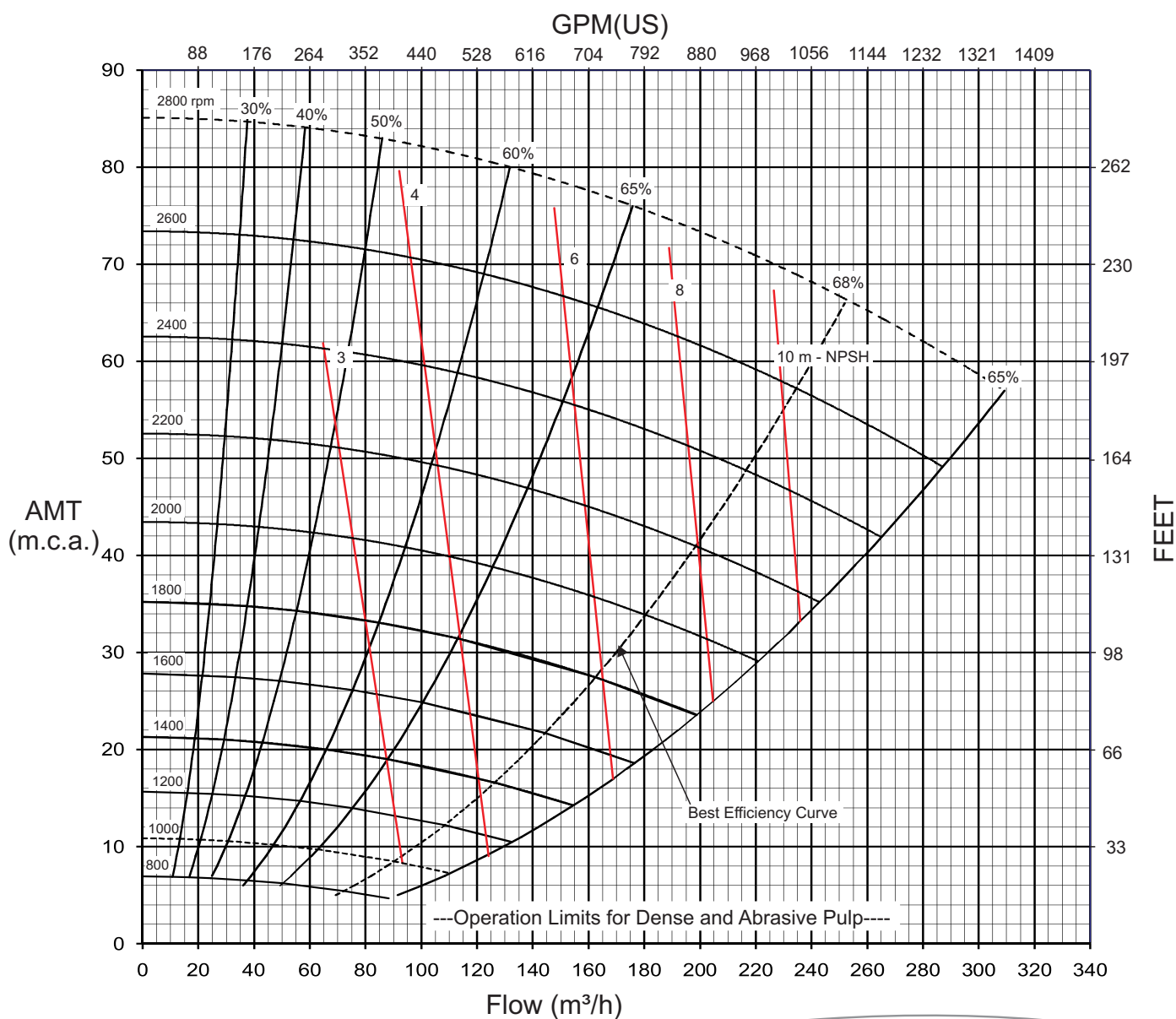


MODEL PUMP

IS M/G 100X75

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	100 mm	ND	245 mm
ND Discharge	75 mm	Type	Close
Material	Cast Iron	Material	Metal
Coating	Metal/Rubber	Free Passage	36 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m/HR = \text{_____} / \text{_____}$, H_w - _____. with Q_m and H_w we find the efficiency in water E_w ____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			



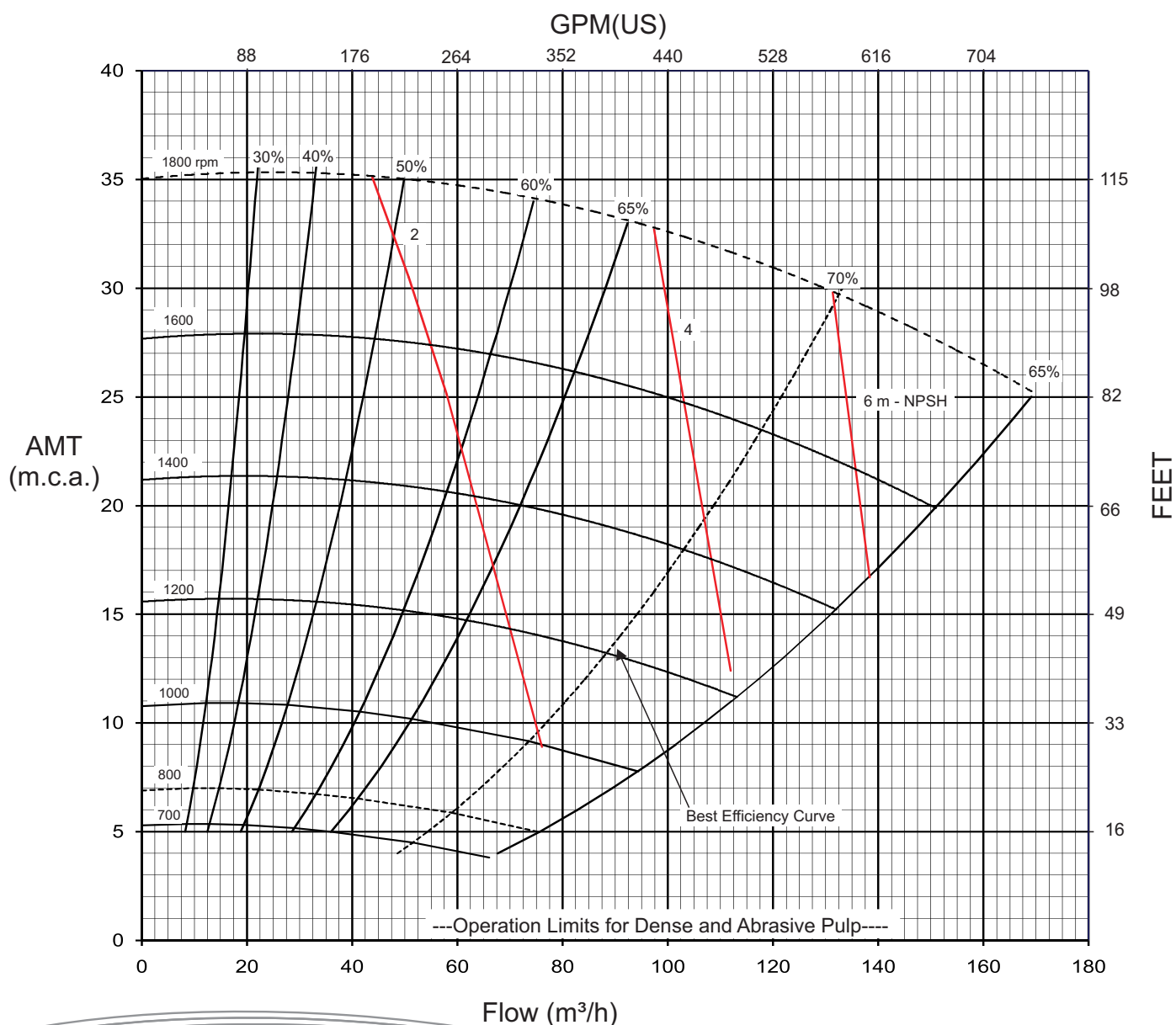


MODEL PUMP

IS B/G 100X75

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	100 mm	ND	245 mm
ND Discharg	75 mm	Type	Close
Material	Cast Iron	Material	Rubber
Coating	Metal/Rubber	Free Passage	28 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____. with Q_m and H_w we find the efficiency in water E_w ____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			



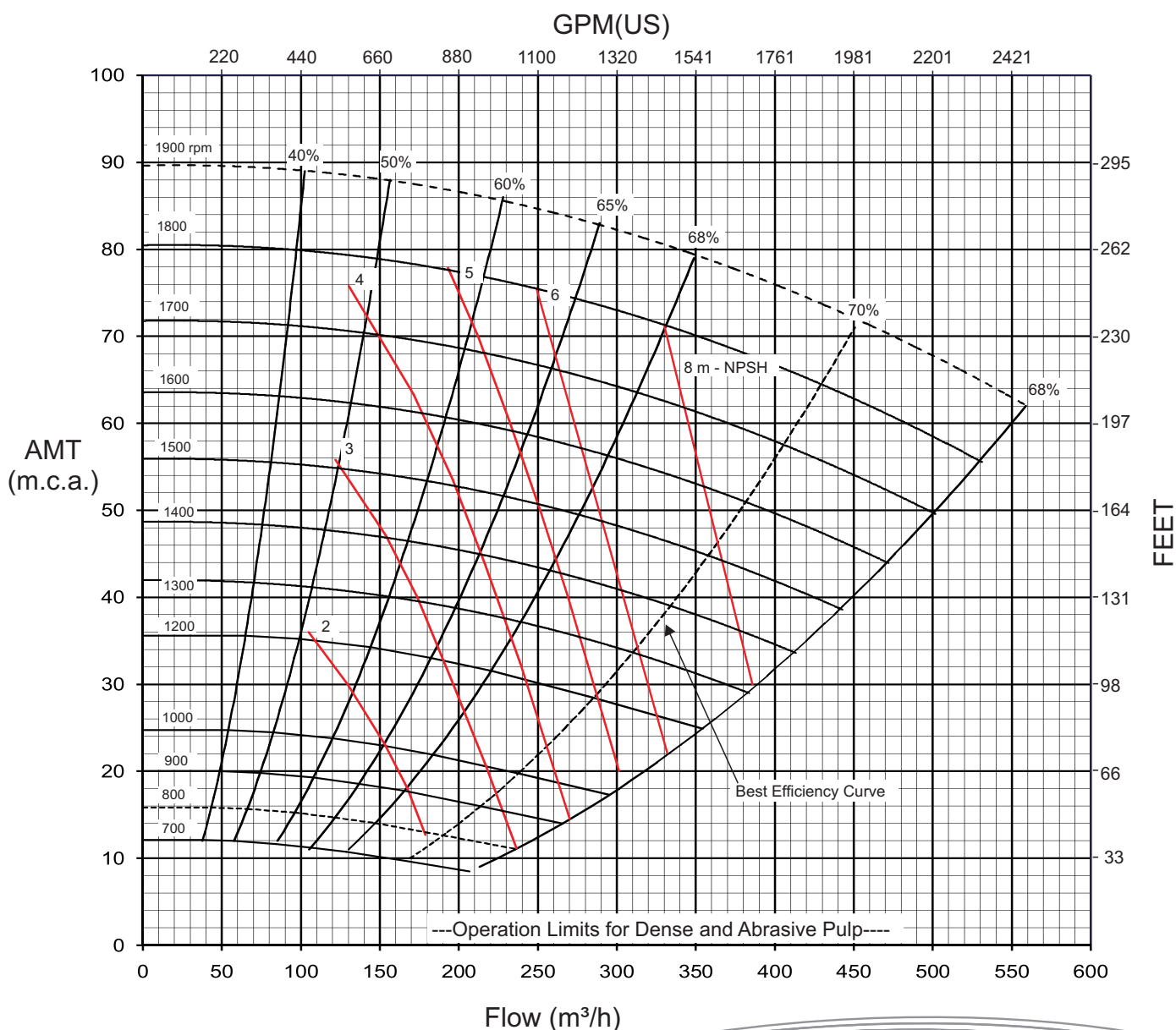


MODEL PUMP

IS M/G 150X100

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	150 mm	ND	365 mm
ND Discharge	100 mm	Type	Close
Material	Cast Iron	Material	Metal
Coating	Metal/Rubber	Free Passage	51 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____. with Q_m and H_w we find the efficiency in water E_w ____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			



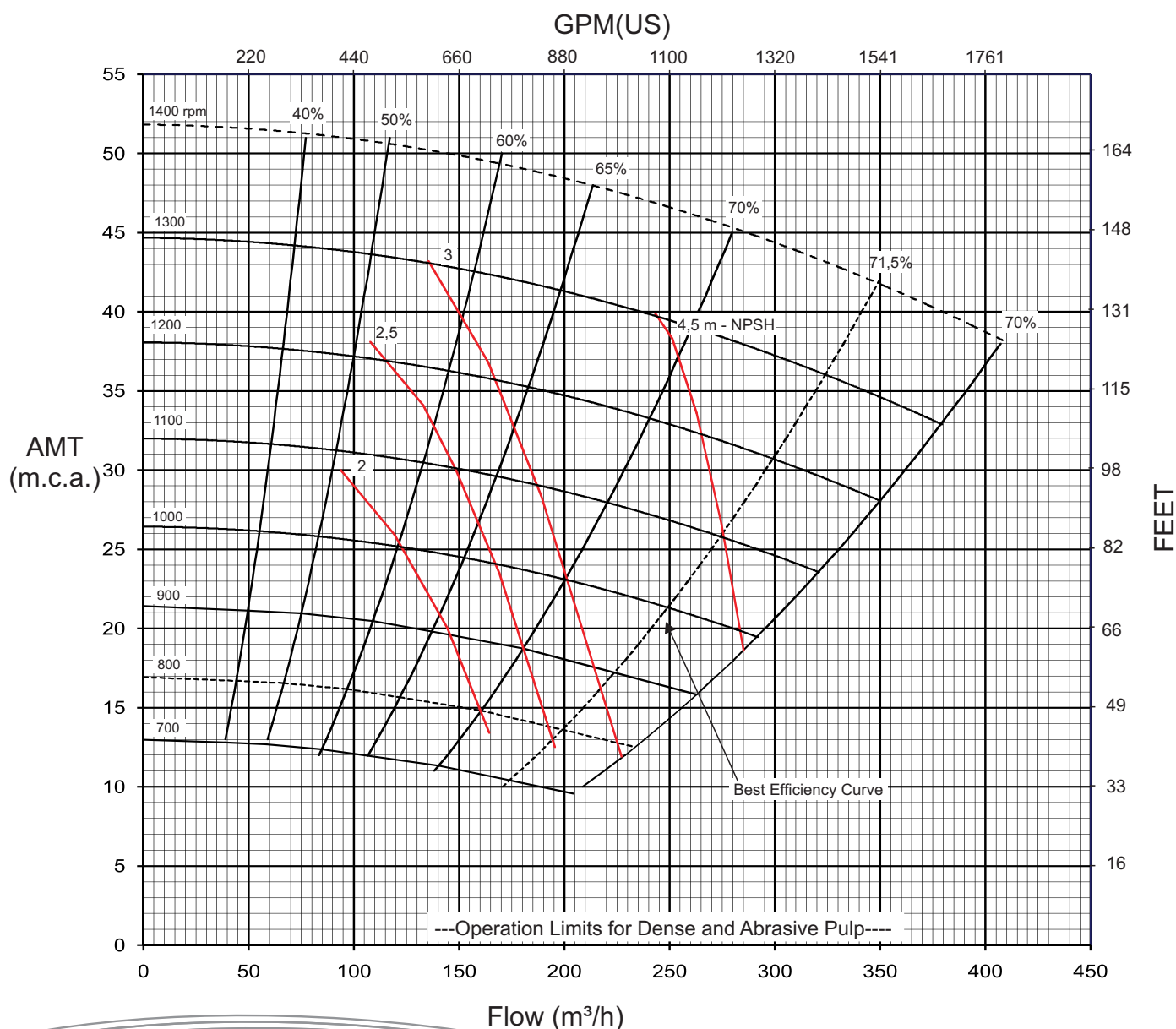


MODEL PUMP

IS B/G 150X100

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	150 mm	ND	365 mm
ND Discharg	100 mm	Type	Close
Material	Cast Iron	Material	Rubber
Coating	Metal/Rubber	Free Passage	33 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____ with Q_m and H_w we find the efficiency in water E_w _____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP - _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			



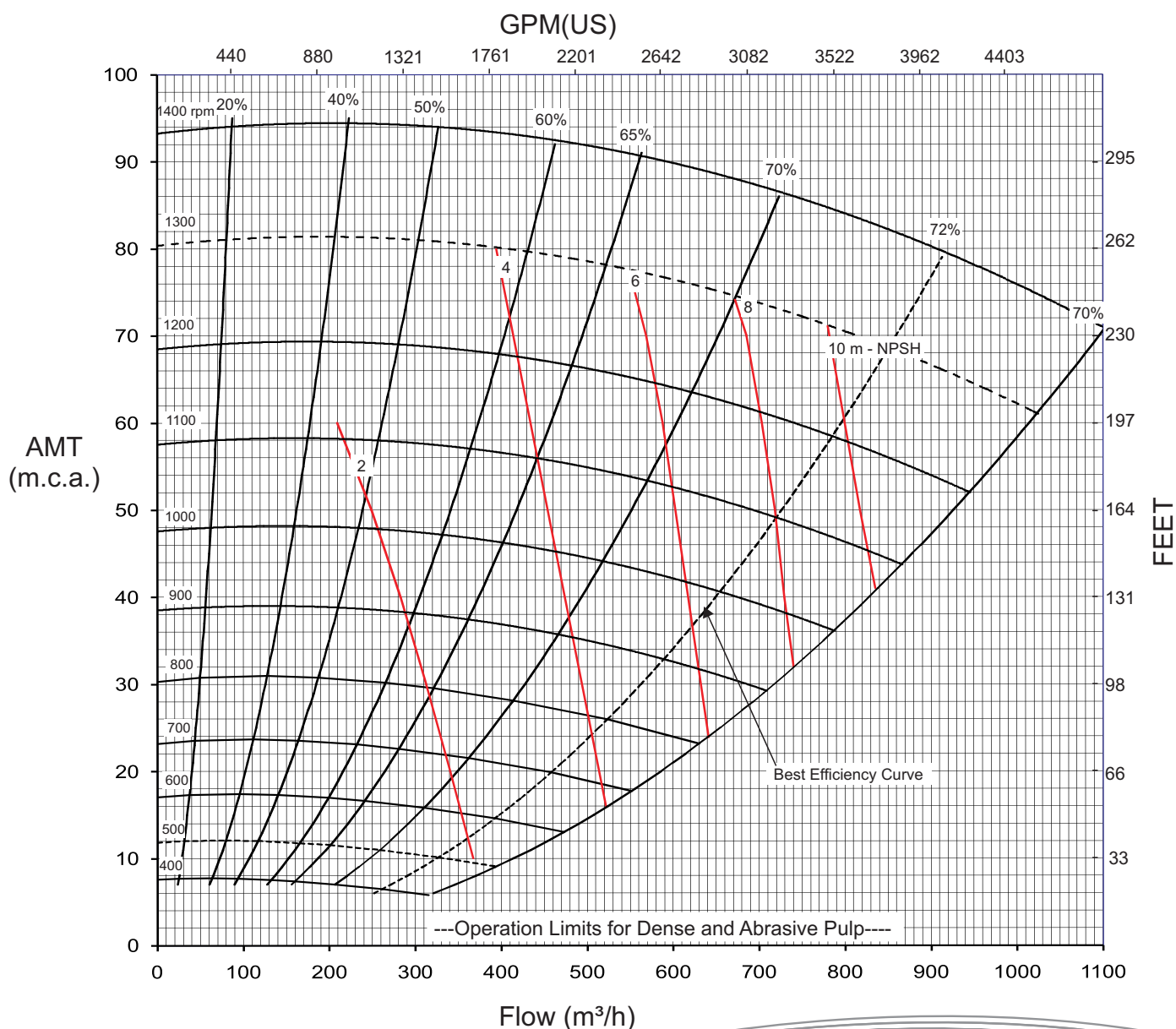


MODEL PUMP

IS M/G 200X150

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	200 mm	ND	510 mm
ND Discharge	150 mm	Type	Close
Material	Cast Iron	Material	Metal
Coating	Metal/Rubber	Free Passage	63 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____. with Q_m and H_w we find the efficiency in water E_w ____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			



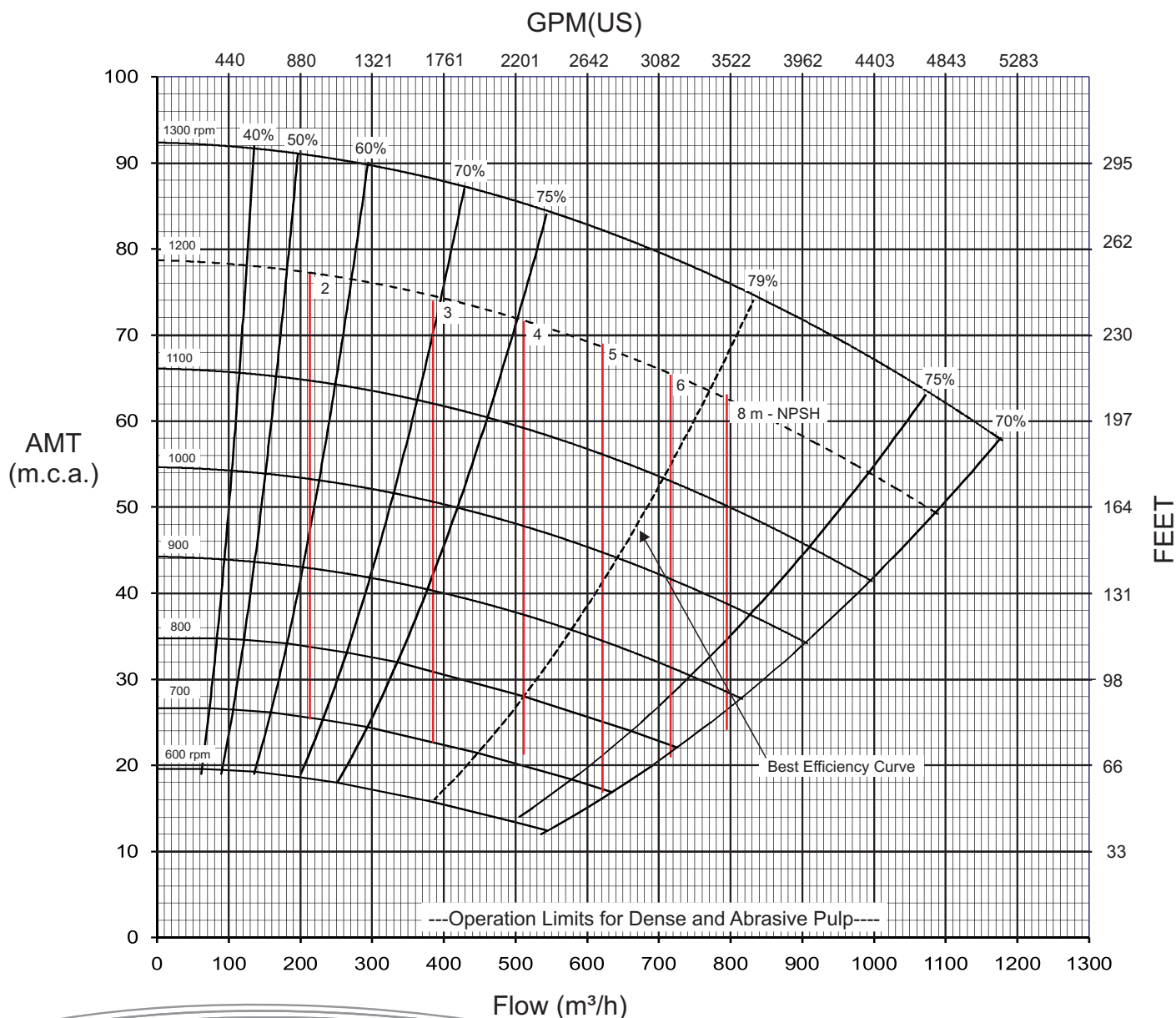


MODEL PUMP

IS M/G 200X150 AE

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 4 Blades	
ND Suction	200 mm	ND	560 mm
ND Discharg	150 mm	Type	Close
Material	Cast Iron	Material	Metal
Coating	Metal/Rubber	Free Passage	57 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____. with Q_m and H_w we find the efficiency in water E_w ____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			



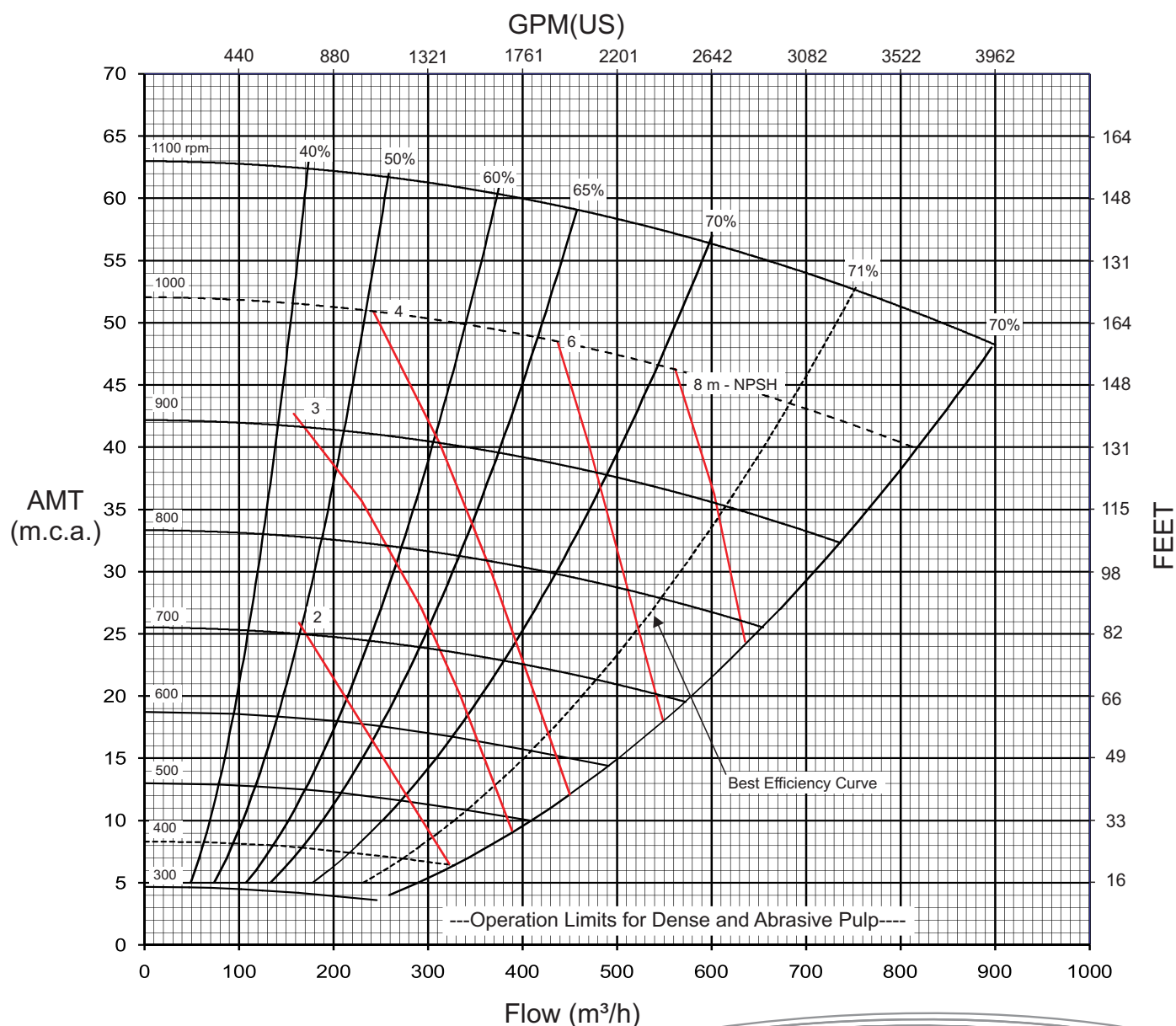


MODEL PUMP

IS B/G 200X150

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	200 mm	ND	510 mm
ND Discharge	150 mm	Type	Close
Material	Cast Iron	Material	Rubber
Coating	Metal/Rubber	Free Passage	59 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____. with Q_m and H_w we find the efficiency in water E_w ____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			



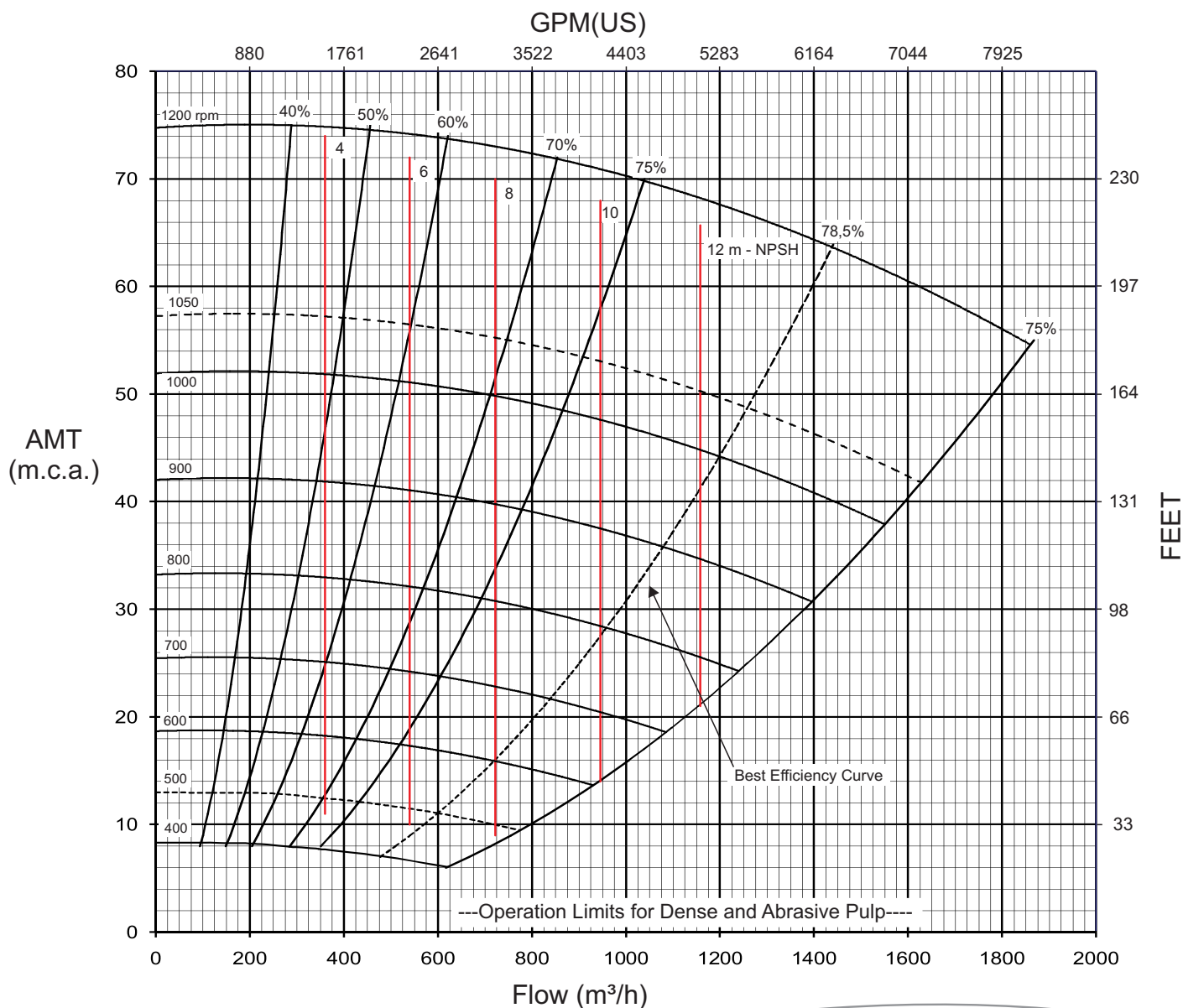


MODEL PUMP

IS M/G 250X200 AE

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 4 Blades	
ND Suction	250 mm	ND	568 mm
ND Discharge	200 mm	Type	Close
Material	Cast Iron	Material	Metal
Coating	Metal/Rubber	Free Passage	65 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____. with Q_m and H_w we find the efficiency in water E_w ____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			



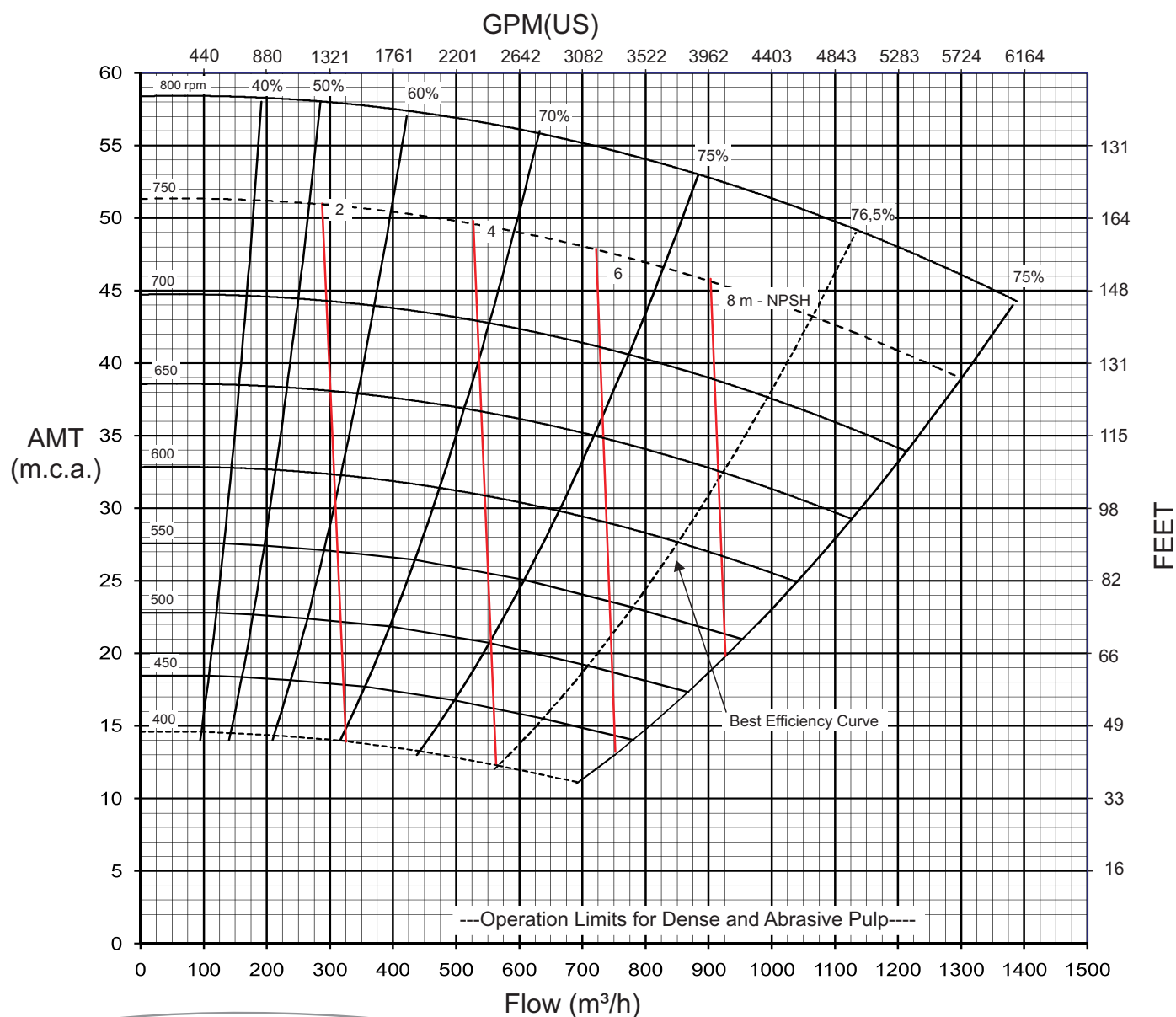


MODEL PUMP

IS B/G 250X200

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	250 mm	ND	686 mm
ND Discharge	200 mm	Type	Close
Material	Cast Iron	Material	Rubber
Coating	Metal/Rubber	Free Passage	76 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____ with Q_m and H_w we find the efficiency in water E_w _____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w =AMT in Water, H_m -AMT in Pulp			



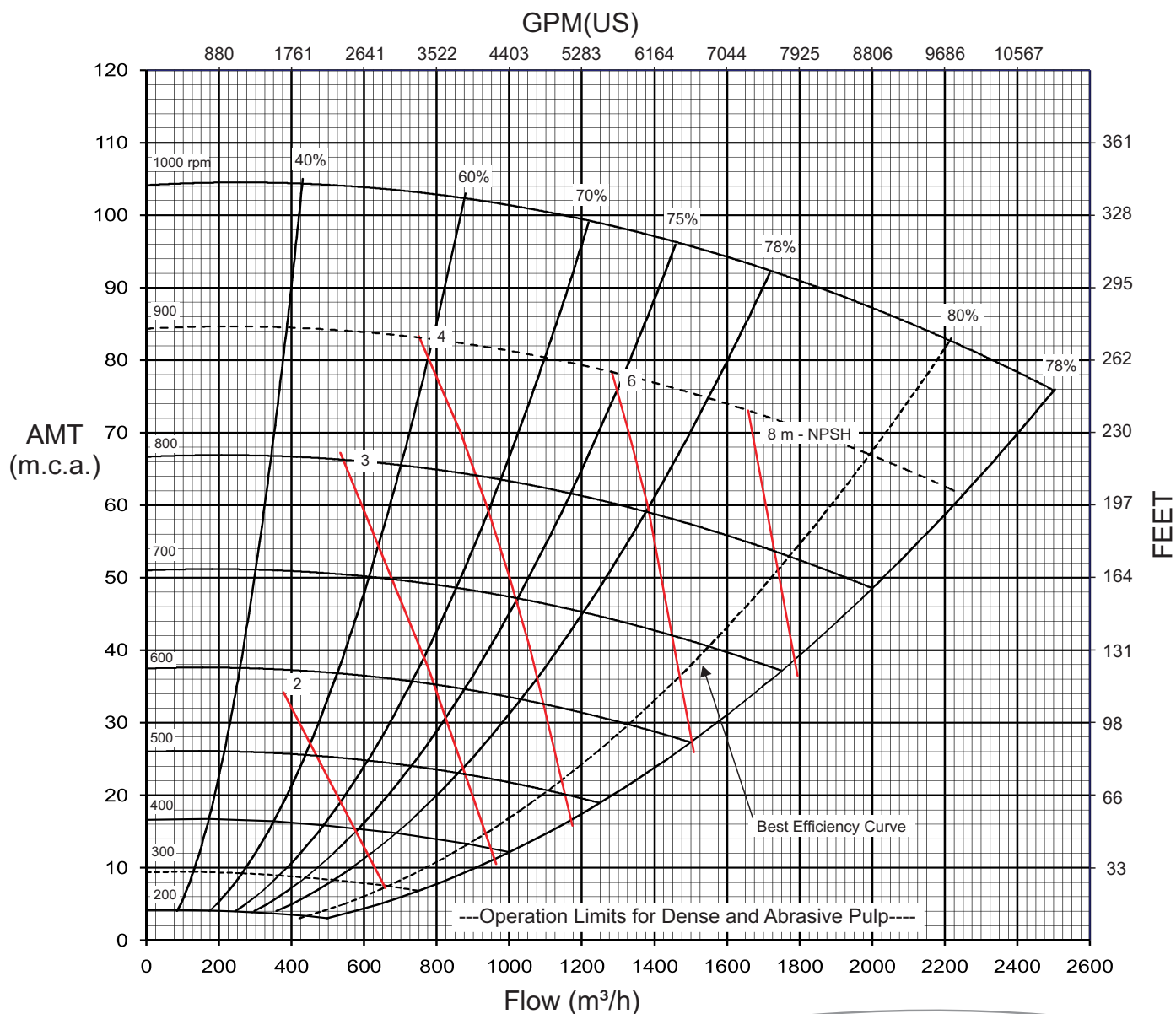


MODEL PUMP

IS M/G 300X250

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	300 mm	ND	762 mm
ND Discharge	250 mm	Type	Close
Material	Cast Iron	Material	Metal
Coating	Metal/Rubber	Free Passage	100 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, $H_w - \text{_____}$ with Q_m and H_w we find the efficiency in water $E_w \text{ _____}$ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: $H_w = \text{AMT in Water}$, $H_m = \text{AMT in Pulp}$			



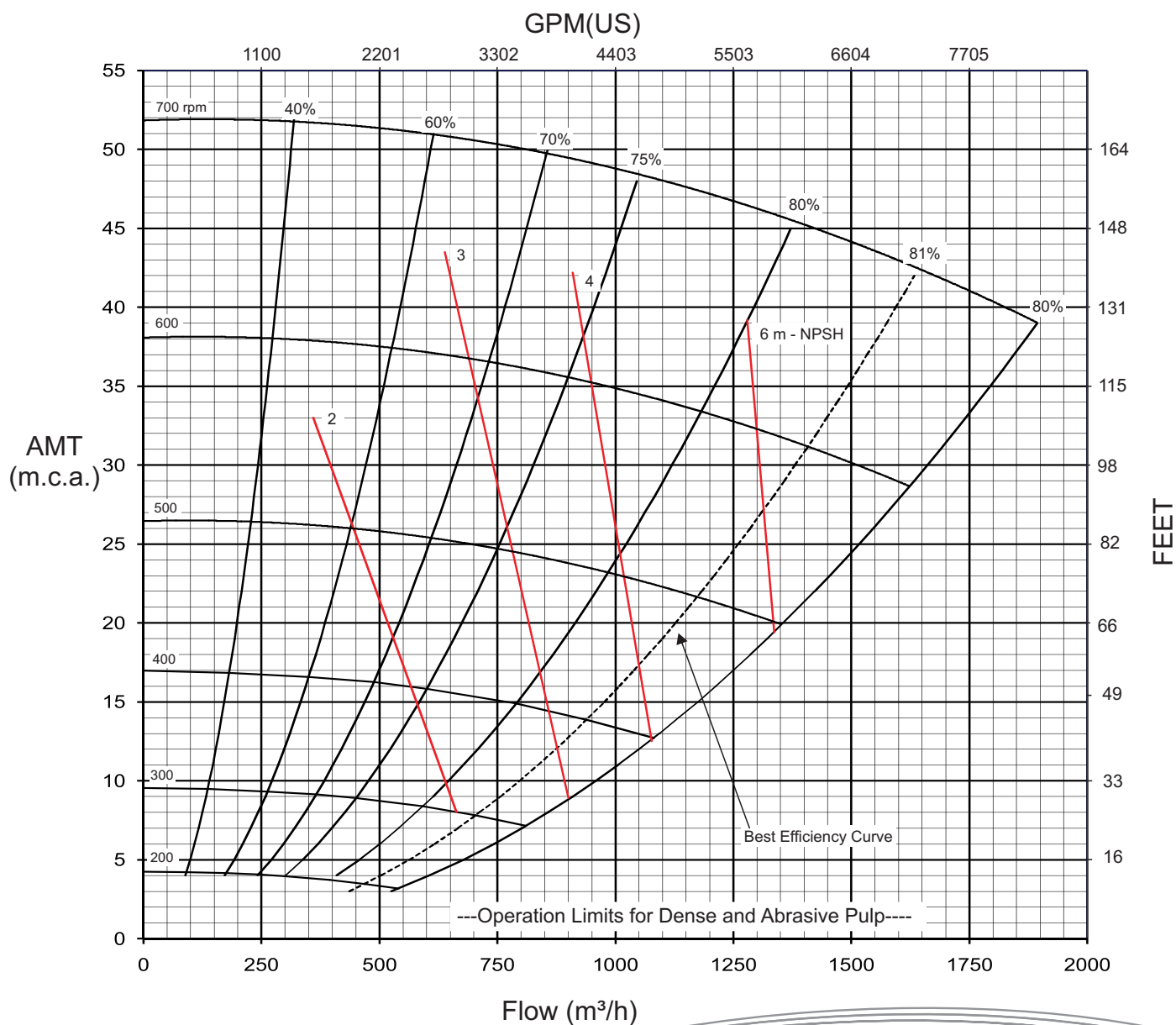


MODEL PUMP

IS B/G 300X250

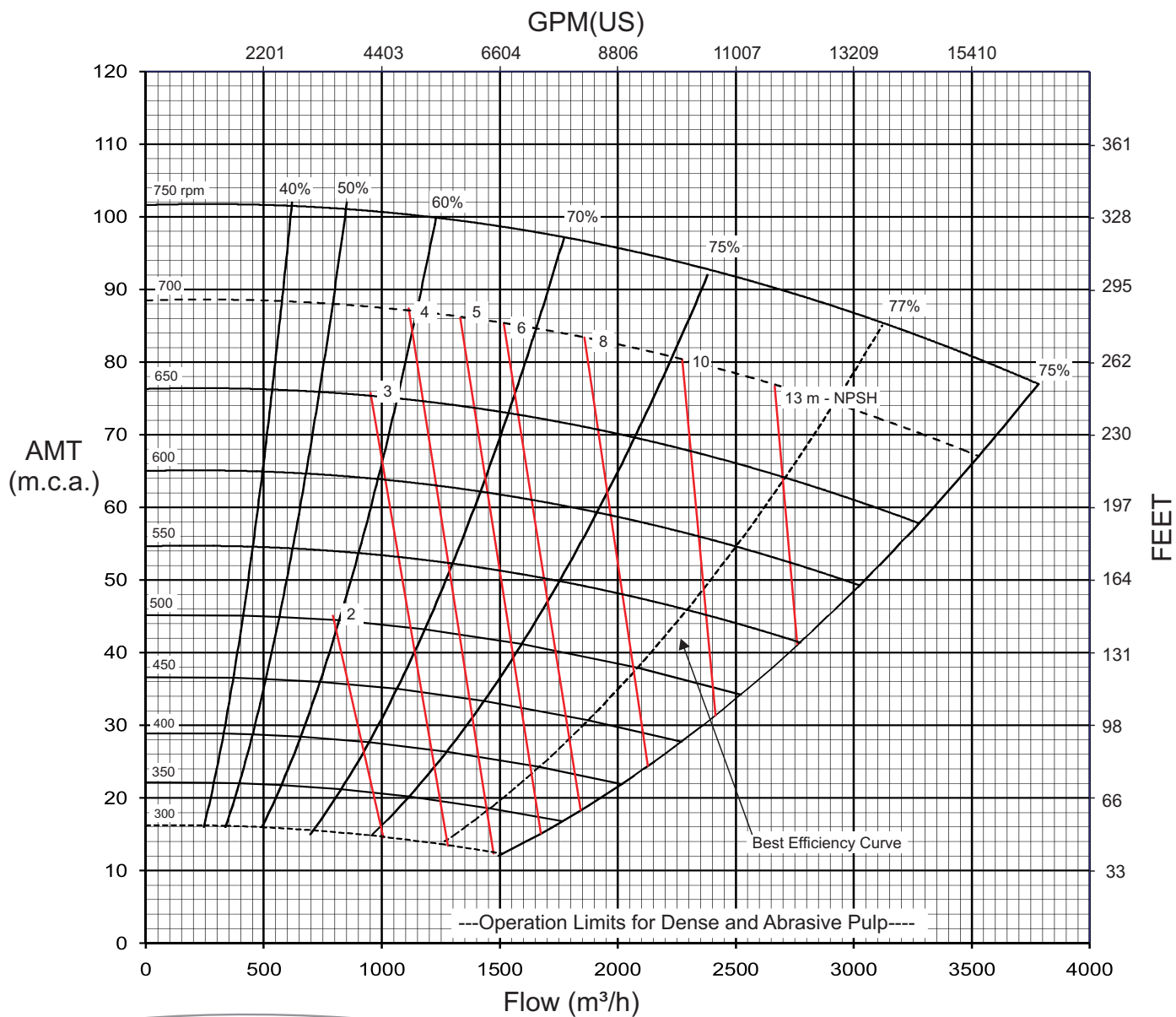
The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	300 mm	ND	762 mm
ND Discharge	250 mm	Type	Close
Material	Cast Iron	Material	Rubber
Coating	Metal/Rubber	Free Passage	26 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____. with Q_m and H_w we find the efficiency in water E_w ____ Through $BHP = (Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP - _____ - _____ hp Where: H_w = AMT in Water, H_m = AMT in Pulp			



The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

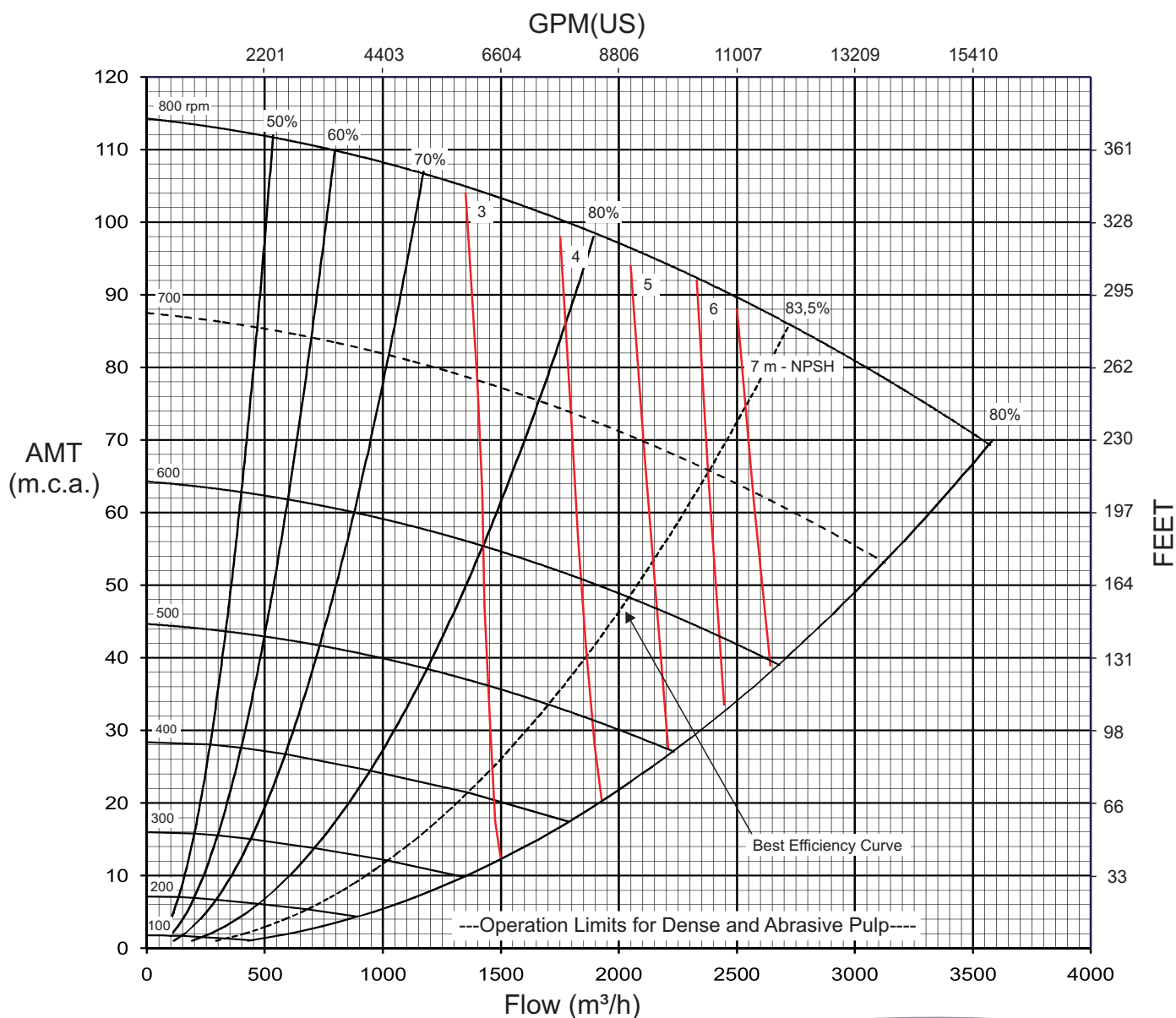
PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	350 mm	ND	965 mm
ND Discharg	300 mm	Type	Close
Material	Cast Iron	Material	Metal
Coating	Metal/Rubber	Free Passage	90 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____.with Q_m and H_w we find the efficiency in water E_w ____ Through BHP = $(Q_m \times H_m \times S_m)$, we find power (270 $\times E_w \times ER$) BHP- _____ - _____ hp Where: H_w=AMT in Water, H_m-AMT in Pulp			



IS M/G 350X300 AE

The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

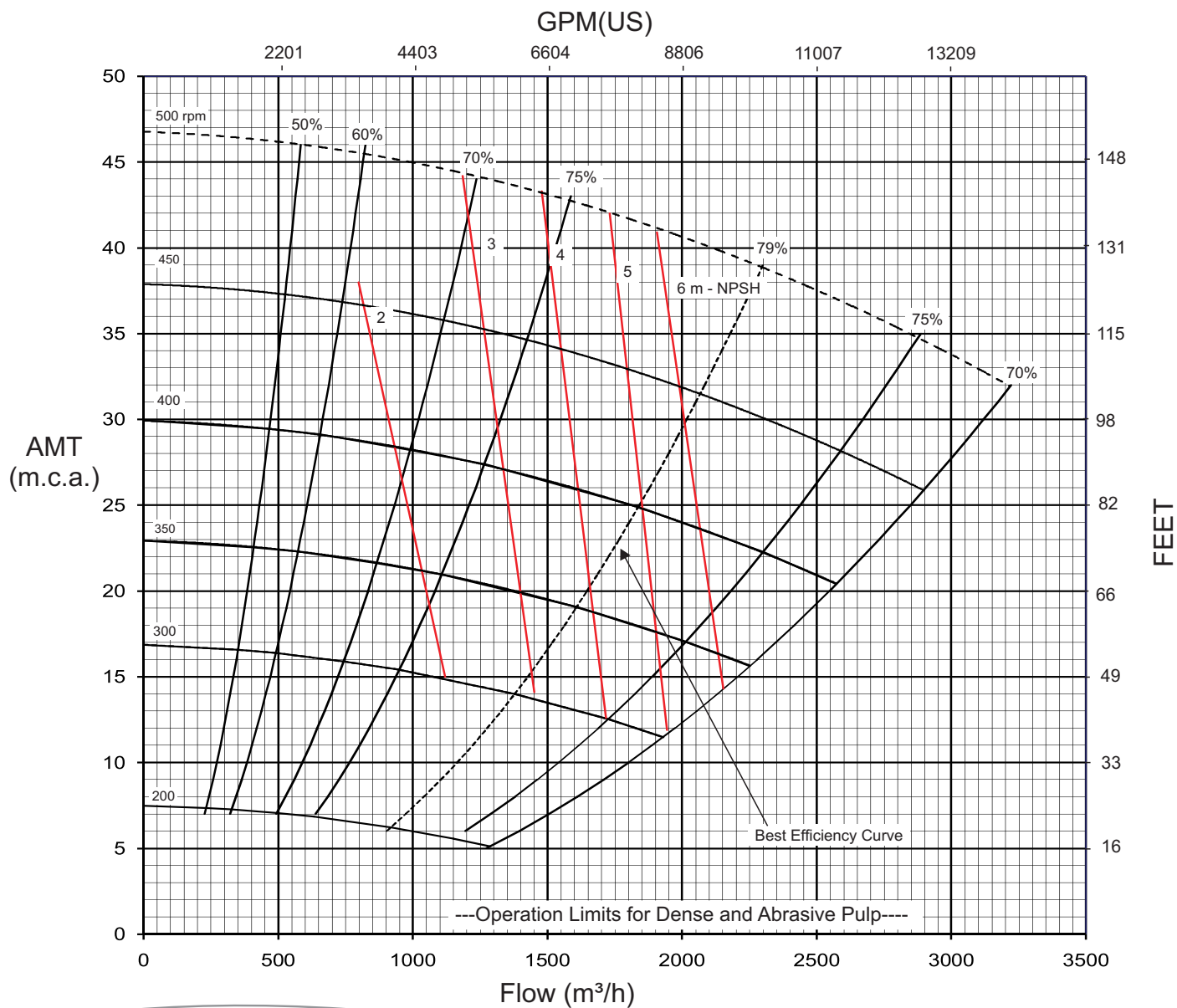
PUMP'S TECHNICAL DATA			
Housing		Impeller - 4 Blades	
ND Suction	350 mm	ND	965 mm
ND Discharg	300 mm	Type	Close
Material	Cast Iron	Material	Metal
Coating	Metal/Rubber	Free Passage	76 mm
POWER CALCULATION			
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____.with Q_m and H_w we find the efficiency in water E_w ____ Through BHP = $(Q_m \times H_m \times S_m)$, we find power $(270 \times E_w \times ER)$ BHP- _____ - _____ hp Where: H_w=AMT in Water, H_m-AMT in Pulp			



The performance curve shown was produced in water, adjustments must be made as a function of density, viscosity, and other effects of suspended solids in pumped liquid.

PUMP'S TECHNICAL DATA			
Housing		Impeller - 5 Blades	
ND Suction	350 mm	ND	965 mm
ND Discharg	300 mm	Type	Close
Material	Cast Iron	Material	Rubber
Coating	Metal/Rubber	Free Passage	104 mm

POWER CALCULATION	
HR-ER- _____; $H_w = H_m / HR = \text{_____} / \text{_____}$, H_w - _____.with Q_m and H_w we find the efficiency in water E_w ____ Through BHP = $(\frac{Q_m \times H_m \times S_m}{270 \times E_w \times ER})$, we find power BHP- _____ - _____ hp	
Where: H_w =AMT in Water, H_m -AMT in Pulp	



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